# MPQ4340/4340J



36V, 4A, Ultra-Low Quiescent Current, Synchronous Step-Down Converter with Multi-Phase Capability, AEC-Q100 Qualified

#### DESCRIPTION

The MPQ4340/4340J is a configurable-frequency (350kHz to 2.5MHz), synchronous step-down switching converter with integrated internal high-side and low side power MOSFETs (HS-FET and LS-FET, respectively). It provides up to 4A of highly efficient output current ( $I_{OUT}$ ) with fixed-frequency zero-delay PWM (ZDP) control for near optimal transient response.

The wide 3.3V to 36V input voltage ( $V_{IN}$ ) range with 42V load dump support accommodates a variety of step-down applications in automotive input environments. A 1µA shutdown current ( $I_{SD}$ ) allows the device to be used in battery-powered applications.

High power conversion efficiency across a wide load range is achieved by scaling down the switching frequency (f<sub>SW</sub>) under light-load conditions to reduce switching and gate driver losses. An open-drain power good (PG) signal indicates whether the output voltage (V<sub>OUT</sub>) is within 94% to 106% of its nominal voltage range. Thermal shutdown provides reliable, fault-tolerant operation. High duty cycle and low-dropout (LDO) mode are provided for automotive cold-crank conditions.

The MPQ4340 is available in a QFN-17 (3mmx4mm) package. The MPQ4340J is available in a QFN-19 (3mmx4mm) package. Both versions are AEC-Q100 qualified.

#### **FEATURES**

#### Designed for Automotive Applications

- Survives 42V Load Dump
- Supports Up to 3.1V Cold Crank
- o Low-Dropout (LDO) Mode
- Up to 4A of Continuous Output Current (I<sub>ΟυΤ</sub>)
- Continuous Operation Up to 36V
- Zero-Delay PWM Control (ZDP)
- Multi-Phase Capability
- o 20ns Minimum On Time
- -40°C to +150°C Junction Temperature Operation Range
- Available in AEC-Q100 Grade 1

## FEATURES (continued)

#### • Increases Battery Life

- 1μA Low Shutdown Current (I<sub>SD</sub>)
- 3µA Sleep Mode Quiescent Current (I<sub>Q</sub>)
- Advanced Asynchronous Modulation (AAM) Mode Increases Efficiency under Light Loads

#### High Performance for Improved Thermals

o Internal 60m $\Omega$  High-Side MOSFET and 35m $\Omega$  Low-Side MOSFET (HS-FET and LS-FET, Respectively)

#### Optimized for EMC/EMI

- 350kHz to 2.5MHz Configurable Switching Frequency (f<sub>SW</sub>)
- Symmetric Vin Pinout
- Frequency Spread Spectrum (FSS) Modulation
- CISPR25 Class 5 Compliant
- MeshConnect<sup>TM</sup> Flip-Chip Package

#### Additional Features

- Fixed Output Options <sup>(1)</sup>: 1V, 1.1V, 1.8V, 2.5V, 3V, 3.3V, 3.8V, 5V
- Synchronizable to External Clock
- o Synchronized Clock Output
- Power Good (PG) Output
- External Soft Start (SS)
- Hiccup Over-Current Protection (OCP)
- Available in a QFN-17 (3mmx4mm)
  Package for MPQ4340 and QFN-19 (3mmx4mm)
  Package for MPQ4340J
  Both with Wettable Flanks

#### **APPLICATIONS**

- Automotive Clusters
- Automotive Infotainment
- Advanced Driver Assistance Systems (ADAS)
- Industrial Power Systems

#### Note

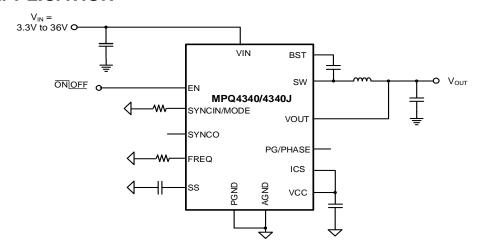
 See the Ordering Information section on page 3 for details regarding the availability of fixed-output versions. Additional output voltages may be available. Contact MPS for details.

All MPS parts are lead-free, halogen-free, and adhere to the RoHS directive. For MPS green status, please visit the MPS website under Quality Assurance. "MPS", the MPS logo, and "Simple, Easy Solutions" are trademarks of Monolithic Power Systems, Inc. or its subsidiaries.

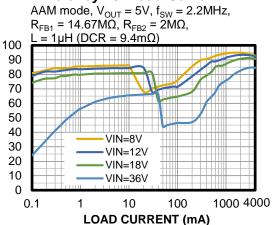


**EFFICIENCY (%)** 

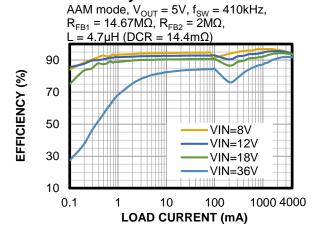
#### **TYPICAL APPLICATION**



#### **Efficiency vs. Load Current**



### **Efficiency vs. Load Current**



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#### ORDERING INFORMATION

Part Number (2) *	Output Voltage	Package	Top Marking	MSL Rating**
MPQ4340GLE-33-AEC1***	Fixed 3.3V	QFN-17 (3mmx4mm)	See Below	1
MPQ4340GLE-5-AEC1***	Fixed 5V	QFN-17 (3mmx4mm)	See Below	1
MPQ4340JGLE-33-AEC1***	Fixed 3.3V	QFN-19 (3mmx4mm)	See Below	1
MPQ4340JGLE-5-AEC1***	Fixed 5V	QFN-19 (3mmx4mm)	See Below	1

<sup>\*</sup> For Tape & Reel, add suffix -Z (e.g. MPQ4340GLE-33-AEC1-Z).

\*\*Moisture Sensitivity Level Rating

\*\*\*Wettable Flank

#### Note:

2) Contact MPS for details regarding other fixed-output versions.

## TOP MARKING (MPQ4340GLE-33-AEC1 and MPQ4340GLE-5-AEC1)

MPYW

4340

LLL

Е

MP: MPS prefix Y: Year code W: Week code 4340: Part number LLL: Lot number E: Wettable flank

## TOP MARKING (MPQ4340JGLE-33-AEC1 and MPQ4340JGLE-5-AEC1)

**MPYW** 

4340

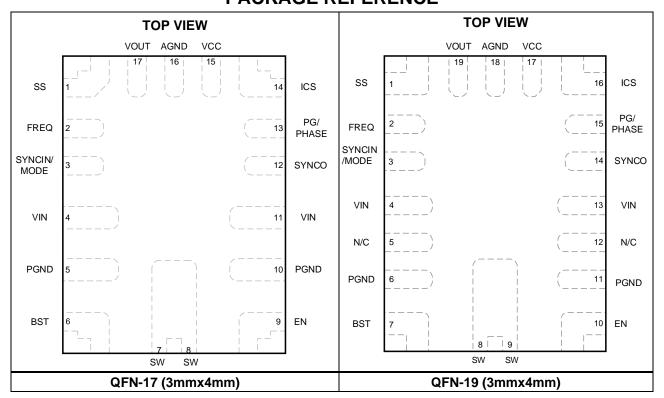
JLLL

E

MP: MPS prefix Y: Year code W: Week code 4340J: Part number LLL: Lot number E: Wettable flank



# **PACKAGE REFERENCE**



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# **PIN FUNCTIONS**

Pin#	Pin# Pin# Name Becariation						
QFN-19	QFN-17	Name	Description				
1	1	SS	<b>Soft-start input.</b> Place a capacitor from the SS pin to ground to set the soft-start time. The MPQ4340/4340J sources $10\mu A$ from SS to the soft-start capacitor (Css) at start-up. As the SS voltage (Vss) rises, the feedback reference voltage (VREF) increases to limit inrush current during start-up.				
2	2	FREQ	<b>Switching frequency configuration.</b> Connect a resistor from the FREQ pin to AGND to set the switching frequency (fsw).				
3	3	SYNCIN/ MODE	<b>SYNC input and MODE selection.</b> Apply a clock signal to the SYNCIN/MODE pin to synchronize the internal f <sub>SW</sub> to the external clock. Use an external clock or pull this pin high to enter forced continuous conduction mode (FCCM). Pull this pin low to enable advanced asynchronous modulation (AAM) mode and pulse skipping under light loads. Do not float this pin.				
4,13	4, 11	VIN	<b>Input supply.</b> The VIN pin supplies power to all the internal control circuitry, as well as the power switch connected to SW. Place a decoupling capacitor from VIN to ground, as close as possible to VIN, to minimize switching spikes.				
5, 12	-	NC	No connection. Float the NC pin.				
6, 11	5, 10	PGND	Power ground.				
7	6	BST	<b>Bootstrap.</b> The BST pin is the positive power supply for the high-side MOSFET (HS-FET) connected to SW. Connect a bypass capacitor between the BST and SW pins. See the Floating Driver and Bootstrap Charging (BST, Pin 6) section on page 45 to calculate the size of this capacitor.				
8, 9	7, 8	SW	Switch node. The SW pin is the internal power switch's output.				
10	9	EN	<b>Enable.</b> Pull EN above the specified threshold (1V) to enable the chip. Pull the EN pin below the specified threshold (0.85V) to shut down the chip. Do not float this pin.				
14	12	SYNCO	<b>SYNC</b> output and mode selection for slave device. When SYNCO is in a high-impedance (Hi-Z) state, the MPQ4340/4340J operates as a master device and the SYNCO pin outputs a clock signal in phase with the internal oscillator signal. In this mode, the pin can be floated. To set the MPQ4340/4340J to operates as a slave device, tie this pin to a low-impedance ground, voltage source, or clock (connected resistor < $25k\Omega$ ). In this mode, SYNCO acts as a mode input pin and cannot be floated.				
15	13	PG/PHASE	<b>Power good output or phase shift.</b> The PG pin's output is an open drain. If the device is in master mode and PG is used, it should be connected to a power source via a pull-up resistor. If the output voltage ( $V_{\text{OUT}}$ ) is within 94% to 106% of the nominal voltage, PG goes high. If $V_{\text{OUT}}$ is above 107% or below 93% of the nominal voltage, PG goes low. If the device is in slave mode, connect a resistor to AGND to set the phase.				
16	14	ICS	<b>Current sharing.</b> For multi-phase applications, connect the ICS pins of the devices in parallel to improve current sharing between different phases. Connect this pin to VCC for single-phase operation. Do not float this pin.				
17	15	VCC	<b>Bias supply.</b> The VCC pin supplies 5V of power to the internal control circuit and gate drivers. Place a decoupling capacitor from VCC to ground, as close as possible to this pin. See the Setting the VCC Capacitor (VCC, Pin 15) section on page 47 to calculate the size of this capacitor.				
18	16	AGND	Analog ground.				
19	17	VOUT	Vout regulation point. Connect the VOUT pin directly to Vout.				



## ABSOLUTE MAXIMUM RATINGS (3) VIN, EN.....-0.3V to +42V SW.....--0.3V to $V_{IN(MAX)} + 0.3V$ BST......V<sub>SW</sub> + 5.5V All other pins.....-0.3V to +6V Continuous power dissipation ( $T_A = 25$ °C) QFN-19 (3mmx4mm) (4) (8) ......4.13W Junction temperature ......150°C Lead temperature......260°C Storage temperature.....-65°C to +150°C ESD Ratings Human body model (HBM) ......Class 2 (5) Charged-device model (CDM) ......Class C2b (6)

**Recommended Operating Conditions** 

Supply voltage (V<sub>IN</sub>) ......3.3V to 36V

Operating junction temp (T<sub>J</sub>).... -40°C to +150°C

#### Thermal Resistance **0**.JA $\theta_{JC}$ QFN-17 (3mmx4mm) JESD51-7.....44.7......5.2....°C/W (7) EVQ4340-L-00A.....29.2.....6.1....°C/W (8) $\psi_{.T}$ JESD51-7......1.2......°C/W (7) EVQ4340-L-00A......6.1......6.1.....°C/W (8) QFN-19 (3mmx4mm) $\theta_{JA}$ $\theta_{JC}$ JESD51-7.....43.6....5.4......°C/W (7) EVQ4340J-L-00A ......30.3....°C/W (8) JESD51-7......0.9.....°C/W (7) EVQ4340J-L-00A......5.17.....°C/W (8)

#### Notes:

- Exceeding these ratings may damage the device.
- The maximum allowable power dissipation is a function of the maximum junction temperature T<sub>J</sub> (MAX), the junction-toambient thermal resistance  $\theta_{JA}$ , and the ambient temperature T<sub>A</sub>. The maximum allowable continuous power dissipation at any ambient temperature is calculated by  $P_D$  (MAX) =  $(T_J)$ (MAX) - T<sub>A</sub>) / θ<sub>JA</sub>. Exceeding the maximum allowable power dissipation can cause excessive die temperature, and the regulator may go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 5) Per AECQ100-002.
- 6) Per AECQ100-011.
- Measured on a JESD51-7, 4-layer PCB. The values given in this table are only valid for comparison with other packages and cannot be used for design purposes. These values were calculated in accordance with JESD51-7, and simulated on a specified JEDEC board. They do not represent the performance obtained in an actual application, the value of  $\theta_{lo}$ shows the thermal resistance from junction-to-case bottom.  $\Psi_{\text{JT}}$ is the characterization parameter from junction-to-case top.
- Measured on an MPS standard EVB: 8.3cmx8.3cm, 2oz. copper thickness, 4-layer PCB. Ψ<sub>JT</sub> is the characterization parameter from junction-to-case top.

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MPQ4340/4340J Rev. 1.0 MonolithicPower.com 2/16/2023



## **ELECTRICAL CHARACTERISTICS**

 $V_{IN} = 12V$ ,  $V_{EN} = 2V$ ,  $T_{J} = -40$ °C to +150°C, typical values are at  $T_{J} = 25$ °C, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units	
Input Supply							
V <sub>IN</sub> minimum operating voltage	V <sub>IN_MIN</sub>				3.3	V	
V <sub>IN</sub> under-voltage lockout (UVLO) rising threshold	VIN_UVLO_RISING		2.8	3	3.2	V	
V <sub>IN</sub> UVLO falling threshold	VIN_UVLO_FALLING		2.6	2.8	3	V	
V <sub>IN</sub> UVLO hysteresis	VIN_UVLO_HYS			200		mV	
VIN quiescent current (9)	lα	$V_{\text{OUT}} = 1.05 \text{ x V}_{\text{SET}}, \text{ no load},$ (sleep mode), $T_{\text{J}} = -40^{\circ}\text{C}$ to $+85^{\circ}\text{C}$	1.9	3	3.6	μA	
		$V_{OUT} = 1.05 \text{ x } V_{SET}, \text{ no load,}$ (sleep mode), $T_J = -40^{\circ}\text{C}$ to +125°C	1.5		15	μA	
VIN quiescent current (switching) (9)	IQ_SLEEP	SYNCIN/MODE = GND (AAM mode), switching, no load, T <sub>J</sub> = -40°C to +85°C	2.4	3.5	4.5	μΑ	
		SYNCIN/MODE = GND (AAM mode), switching, no load, T <sub>J</sub> = -40°C to +125°C	2		16	μΑ	
VIN active current (no switching)	I <sub>Q_ACTIVE</sub>	SYNCIN/MODE = VCC (CCM), no switching		1200		μA	
VIN shutdown current	I <sub>SD</sub>	EN = 0V, T <sub>J</sub> = 25°C EN = 0V		1	3 11	μA μA	
VIN over-voltage protection (OVP) threshold	VIN_OVP_RISING	LIV - OV	36	38	40	V	
VIN OVP hysteresis	V <sub>IN_OVP_HYS</sub>			10		V	
Enable (EN)			I.				
EN rising threshold	V <sub>EN_RISING</sub>		0.8	1.0	1.2	V	
EN falling threshold	V <sub>EN_FALLING</sub>		0.65	0.85	1.05	V	
EN hysteresis voltage	V <sub>EN_HYS</sub>			150		mV	
Soft Start (SS) and VCC							
VCC voltage	Vcc	Ivcc = 0	4.7	5.0	5.3	V	
VCC regulation		I <sub>VCC</sub> = 0mA and 30mA			1	%	
VCC current limit	ILIMIT_VCC	Vcc = 4V	50	100		mA	
VCC current limit		Vcc = 0V		70		mA	
Soft-start current	Iss	$V_{SS} = 0V$		10		μA	
BST							
BST - SW refresh rising threshold	V <sub>BST-SW_</sub> RISING			2.5	2.9	V	
BST - SW refresh falling threshold	VBST-SW_FALLING			2.3	2.7	V	
BST - SW refresh hysteresis	V <sub>BST-SW_HYS</sub>			0.2		V	

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## **ELECTRICAL CHARACTERISTICS** (continued)

 $V_{IN} = 12V$ ,  $V_{EN} = 2V$ ,  $T_{J} = -40$ °C to +150°C, typical values are at  $T_{J} = 25$ °C, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units	
Switches and Frequency							
Switching frequency	fsw	$R_{FREQ} = 86.6k\Omega$	370	410	450	kHz	
		$R_{FREQ} = 33k\Omega$	950	1050	1150	kHz	
		$R_{FREQ} = 15k\Omega$	1980	2200	2420	kHz	
Minimum on time	ton_min			20	35	ns	
Minimum off time	t <sub>OFF_MIN</sub>			120	140	ns	
Switch leakage current	Isw_Lkg			0.01	5	μΑ	
High-side MOSFET (HS-FET) on resistance	R <sub>DS(ON)_</sub> HS	V <sub>BST</sub> - V <sub>SW</sub> = 5V		60	110	mΩ	
Low-side MOSFET (LS-FET) on resistance	R <sub>DS(ON)_</sub> LS	Vcc = 5V		35	60	mΩ	
Output and Regulation							
Output voltage (Vout) accuracy	Vouт	$T_J = 25^{\circ}C$	3260	3300	3340	mV	
of 3.3V fixed-output version	VOUT	$T_{J} = -40^{\circ}\text{C to } +150^{\circ}\text{C}$	3230	3300	3370	mV	
V <sub>OUT</sub> accuracy of 5V fixed-	\/	T <sub>J</sub> = +25°C	4940	5000	5060	mV	
output version	Vouт	$T_{J} = -40^{\circ}\text{C to } +150^{\circ}\text{C}$	4900	5000	5100	mV	
Vout current	Іνоυт	Vout = Vout_reg		300		nA	
V <sub>OUT</sub> discharge	Idischarge	EN = 0V, V <sub>OUT</sub> = 0.3V, V <sub>IN</sub> = 3.3V to 36V	1.8			mA	
Power Good (PG)							
DC riging throubold	PGvth_rising	Vout rising	91	94	97	- %	
PG rising threshold		Vout falling	103	106	109		
DC falling throubold	PG <sub>VTH_FALLING</sub>	Vout falling	90	93	96		
PG falling threshold		V <sub>OUT</sub> rising	104	107	110		
PG trip threshold hysteresis	PGvth_Hys			1		%	
PG output voltage low	V <sub>PG_LOW</sub>	Isink = 1mA		0.1	0.3	V	
PG rising deglitch	tpg_r_deglitch			50		μs	
PG falling deglitch	t <sub>PG_F_DEGLITCH</sub>			50		μs	
<b>Current Sharing</b>							
Current-sharing gain	Gcs			100		mV/A	
SYNCIN and SYNCO							
SYNCIN/MODE voltage rising threshold	Vsync_rising		1.8			V	
SYNCIN/MODE voltage falling threshold	VSYNC_FALLING				0.4	V	
SYNCIN/MODE timeout	t <sub>MODE</sub>	SYNCIN/MODE low to DCM		41		μs	
SYNCIN clock range	f <sub>SYNC</sub>	% of freerunning frequency	90		115	%	
SYNCO high voltage	Vsynco_High	Isynco = -1mA	3.3	5		V	
SYNCO low voltage	V <sub>SYNCO_LOW</sub>	I <sub>SYNCO</sub> = 1mA			0.4	V	



## **ELECTRICAL CHARACTERISTICS** (continued)

 $V_{IN}$  = 12V,  $V_{EN}$  = 2V,  $T_{J}$ = -40°C to +150°C, typical values are at  $T_{J}$  = 25°C, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units	
Protections							
High-side (HS) current limit	ILIMIT_HS	Duty cycle = 30%	6.3	7.7	9.7	Α	
Low-side (LS) valley current limit (9)	ILIMIT_LS		4.1	5.9	7.6	А	
Zero-current detection (ZCD) threshold	Izcd	AAM mode	-0.05	0.1	+0.25	Α	
LS reverse current limit	ILIMIT_REVERSE	FCCM		4		Α	
Thermal shutdown (9)	T <sub>SD</sub>		150	170		°C	
Thermal shutdown hysteresis (9)	T <sub>SD_HYS</sub>			20		°C	

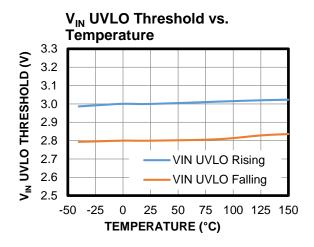
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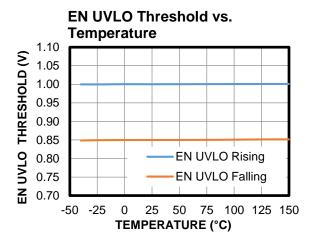
<sup>9)</sup> Guaranteed by design and characterization. Not tested in production.

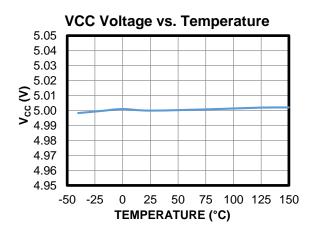


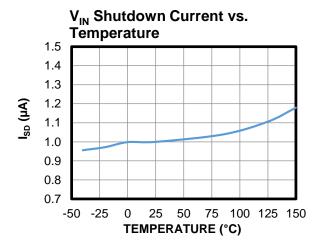
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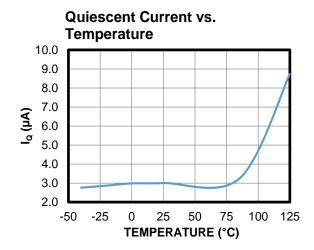
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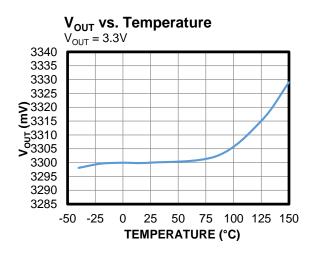








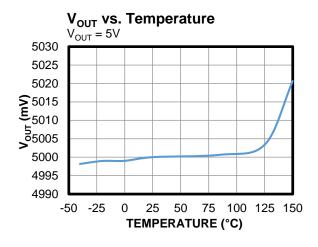


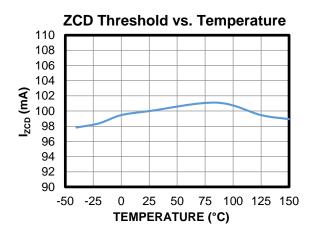


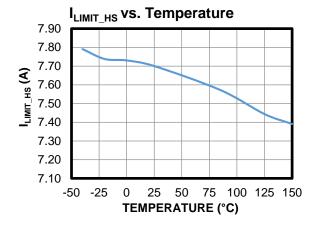


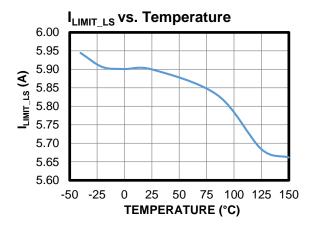
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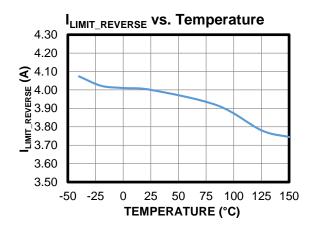
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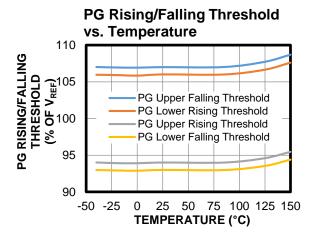








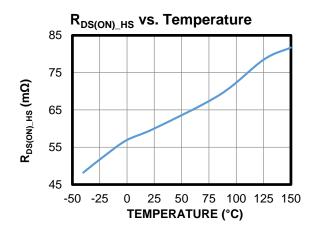


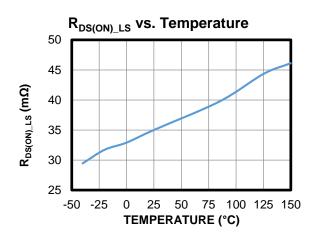


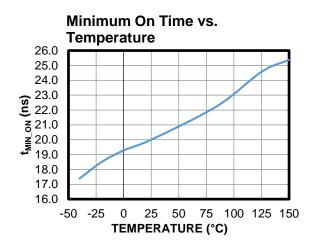


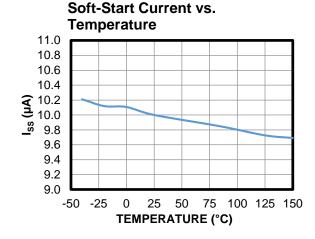
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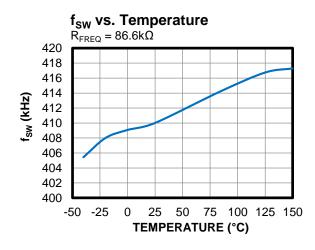
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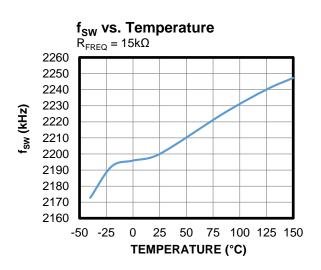








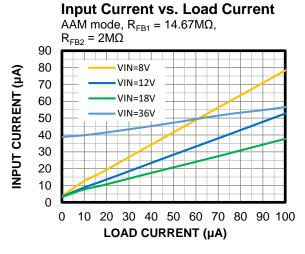


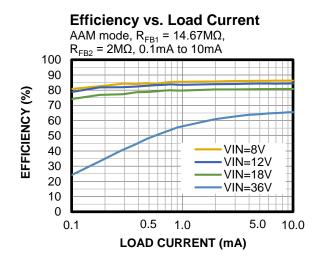


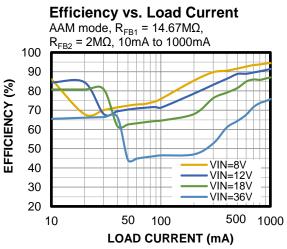


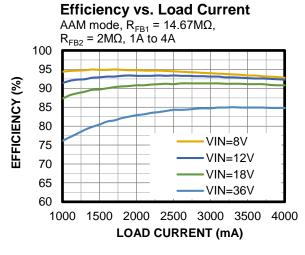
#### TYPICAL PERFORMANCE CHARACTERISTICS

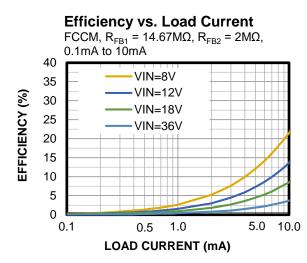
 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H (DCR = 9.4m $\Omega$ ),  $f_{SW}$  = 2.2MHz, 1-phase,  $T_A$  = 25°C, unless otherwise noted.

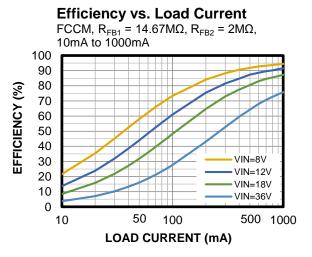






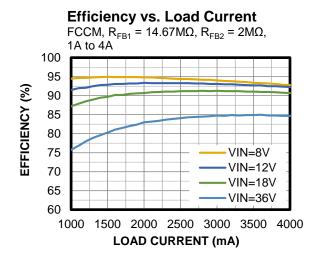


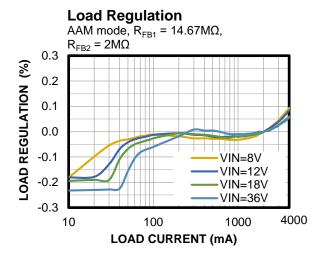


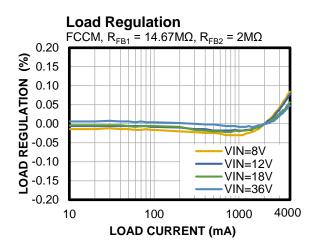


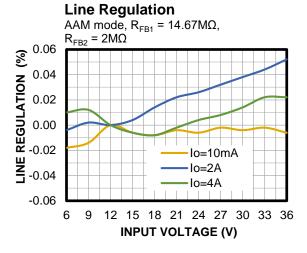


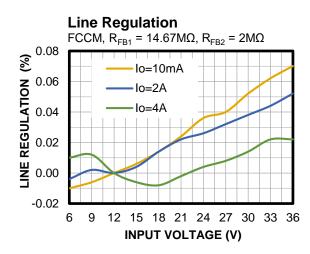
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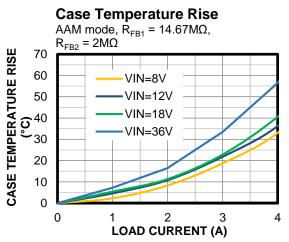






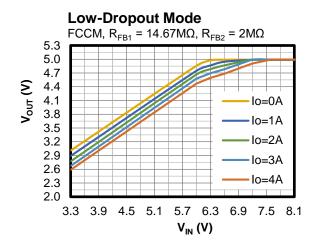


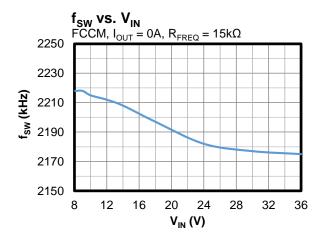






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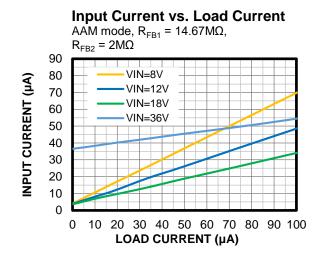


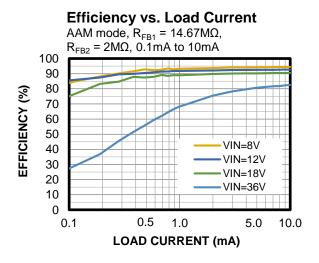


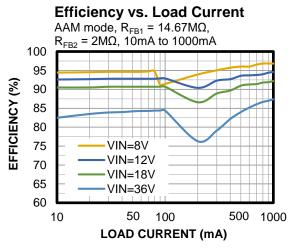
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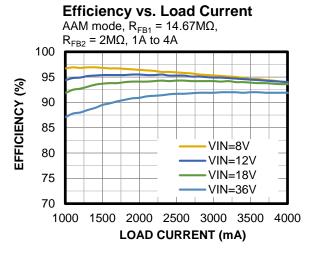


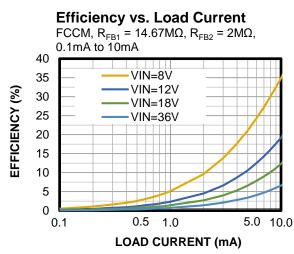
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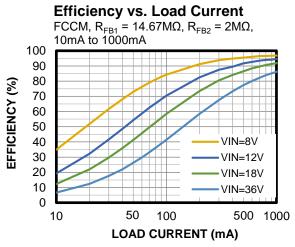






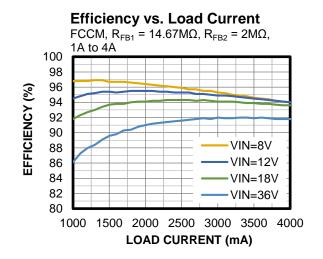


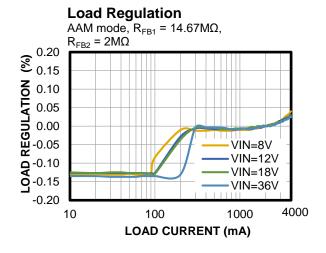


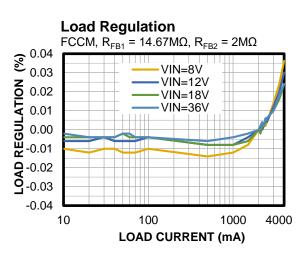


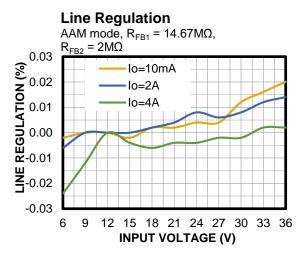


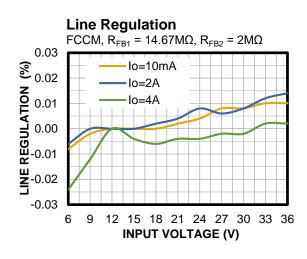
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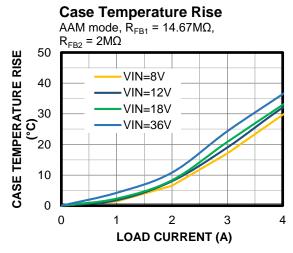






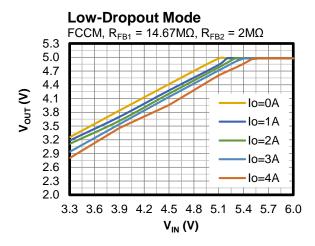


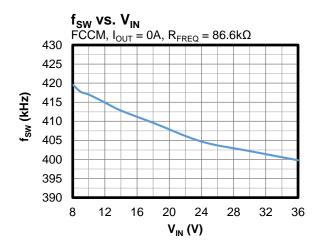






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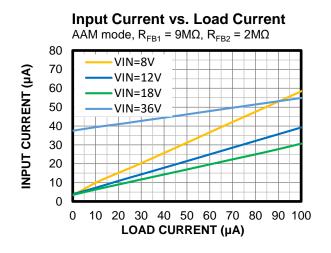


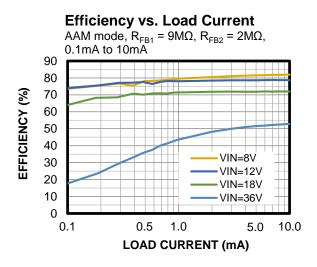


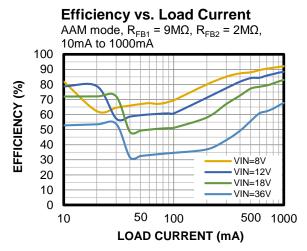
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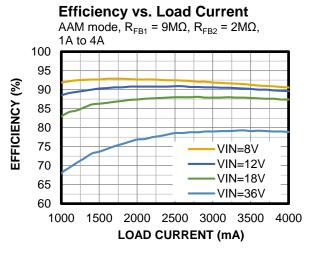


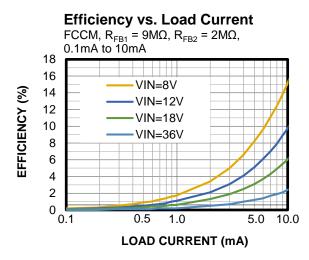
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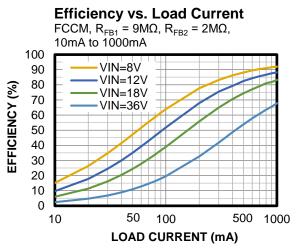






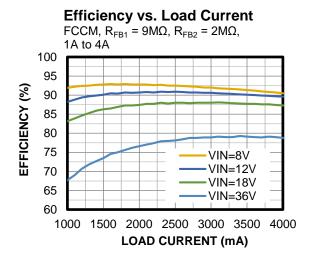


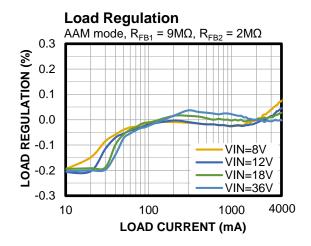


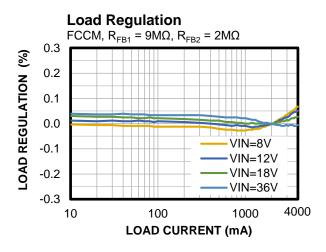


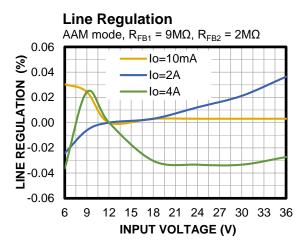


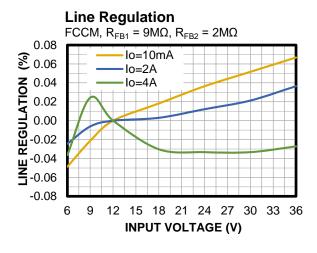
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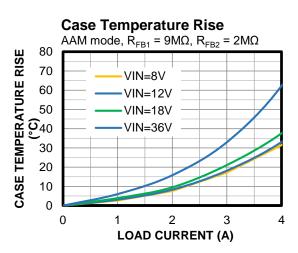






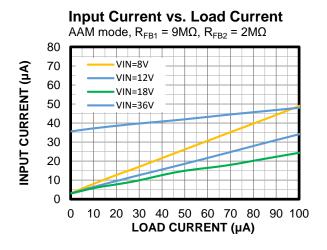


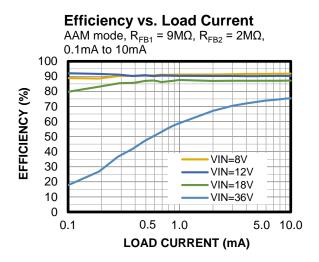


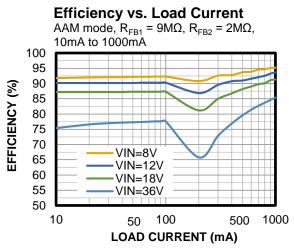


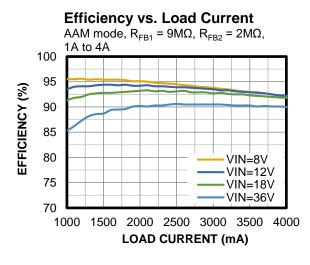


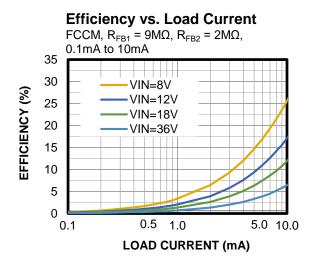
 $V_{\text{IN}}$  = 12V,  $V_{\text{OUT}}$  = 3.3V, L = 4.7 $\mu$ H (DCR = 14.4 $m\Omega$ ),  $f_{\text{SW}}$  = 410kHz, 1-phase,  $T_{\text{A}}$  = 25°C, unless otherwise noted.

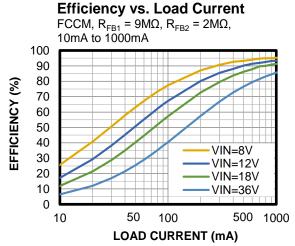






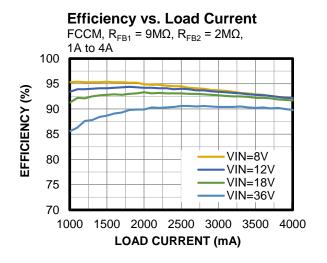


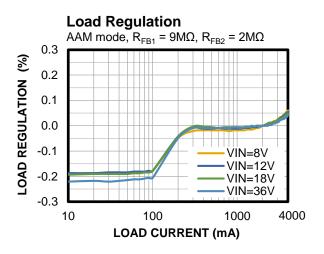


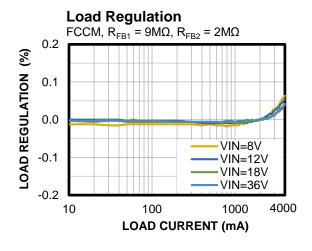


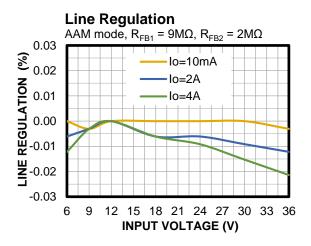


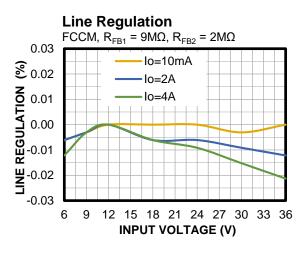
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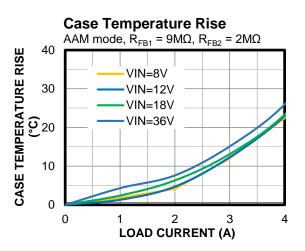








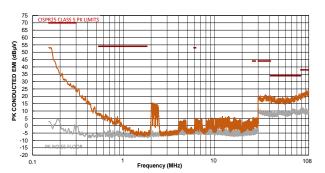




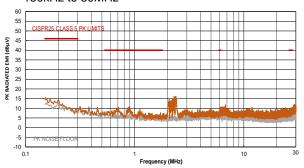


 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H,  $f_{SW}$  = 2.2MHz,  $I_{OUT}$  = 4A, AAM mode, 1-phase,  $T_A$  = 25°C, unless otherwise noted. (10)

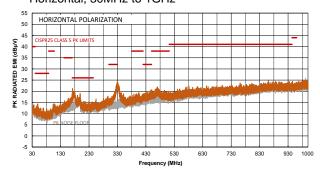
# CISPR25 Class 5 Peak Conducted Emissions 150kHz to 108MHz



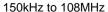
# CISPR25 Class 5 Peak Radiated Emissions 150kHz to 30MHz

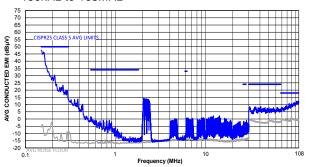


#### CISPR25 Class 5 Peak Radiated Emissions Horizontal, 30MHz to 1GHz

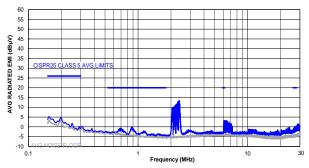


# **CISPR25 Class 5 Average Conducted Emissions**

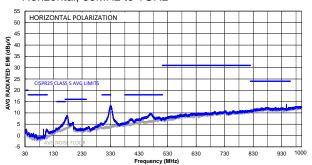




#### CISPR25 Class 5 Average Radiated Emissions 150kHz to 30MHz



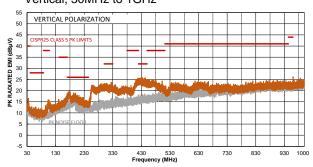
#### CISPR25 Class 5 Average Radiated Emissions Horizontal, 30MHz to 1GHz



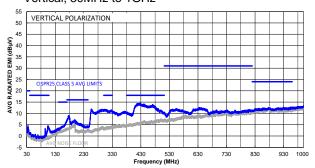


 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H,  $f_{SW}$  = 2.2MHz,  $I_{OUT}$  = 4A, AAM mode, 1-phase,  $T_A$  = 25°C, unless otherwise noted. (10)

#### CISPR25 Class 5 Peak Radiated Emissions Vertical, 30MHz to 1GHz



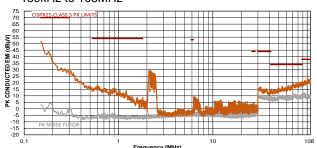
# CISPR25 Class 5 Average Radiated Emissions Vertical, 30MHz to 1GHz





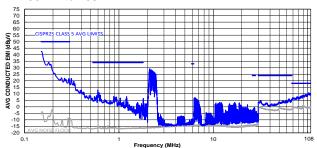
 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ , L = 1 $\mu$ H,  $f_{SW} = 2.2MHz$ ,  $I_{OUT} = 8A$ , AAM mode, 2-phase,  $T_A = 25$ °C, unless otherwise noted. (11)

#### **CISPR25 Class 5 Peak Conducted Emissions** 150kHz to 108MHz

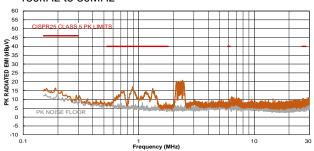


# 150kHz to 108MHz

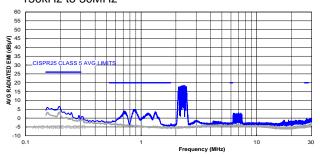
**CISPR25 Class 5 Average Conducted Emissions** 



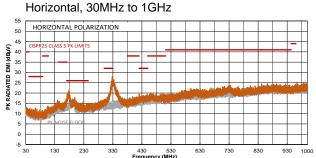
#### **CISPR25 Class 5 Peak Radiated Emissions** 150kHz to 30MHz



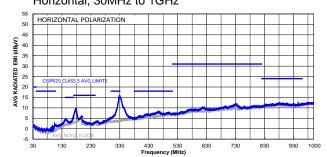
#### **CISPR25 Class 5 Average Radiated Emissions** 150kHz to 30MHz



## **CISPR25 Class 5 Peak Radiated Emissions**



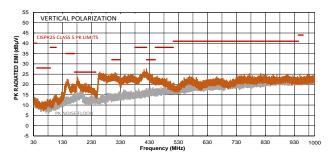
#### CISPR25 Class 5 Average Radiated Emissions Horizontal, 30MHz to 1GHz



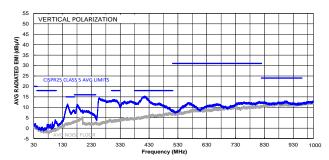


 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H,  $f_{SW}$  = 2.2MHz,  $I_{OUT}$  = 8A, AAM mode, 2-phase,  $T_A$  = 25°C, unless otherwise noted. (11)

#### CISPR25 Class 5 Peak Radiated Emissions Vertical, 30MHz to 1GHz



# CISPR25 Class 5 Average Radiated Emissions Vertical, 30MHz to 1GHz

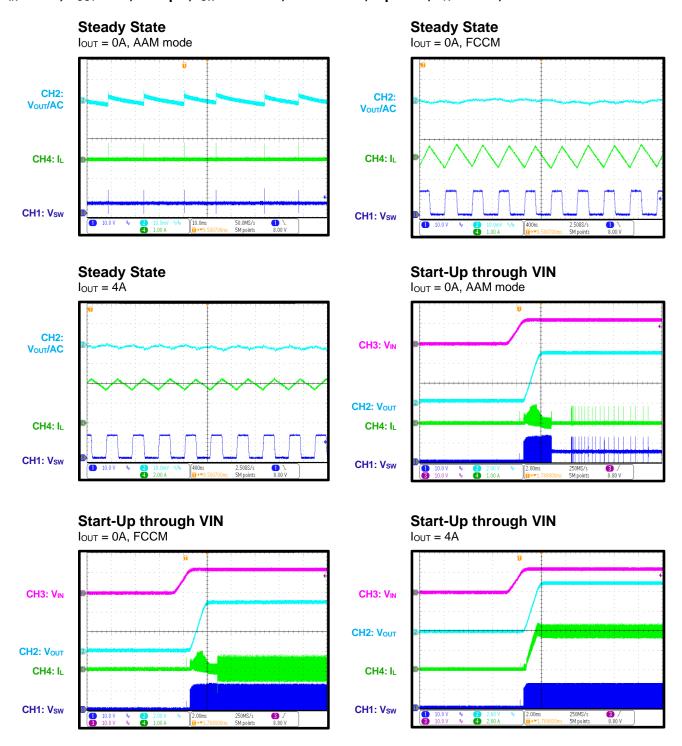


#### Notes:

- 10) The EMC test results are based on the typical application circuit with EMI filters (see Figure 15 on page 52).
- 11) The EMC test results are based on the typical application circuit with EMI filters (see Figure 17 on page 53).

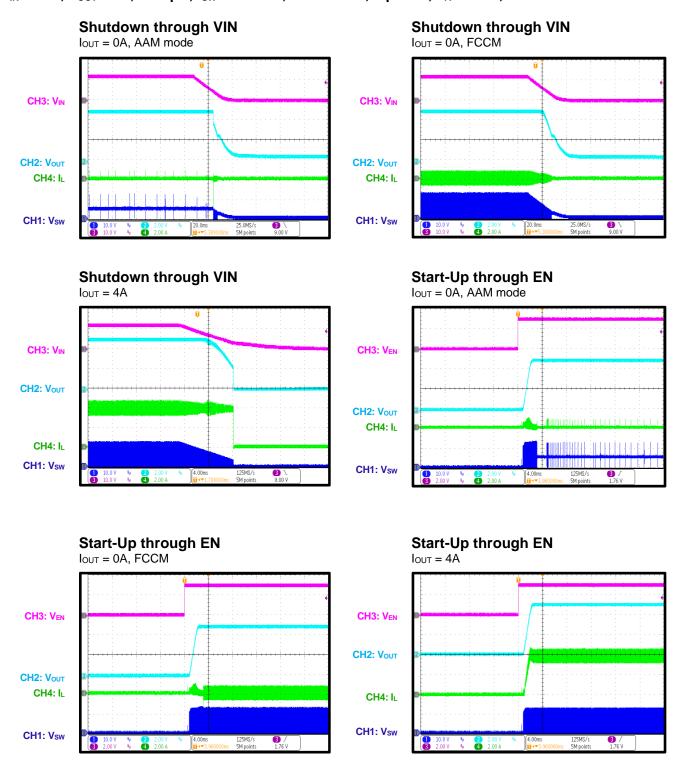


 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H,  $f_{SW}$  = 2.2MHz, AAM mode, 1-phase,  $T_A$  = 25°C, unless otherwise noted.



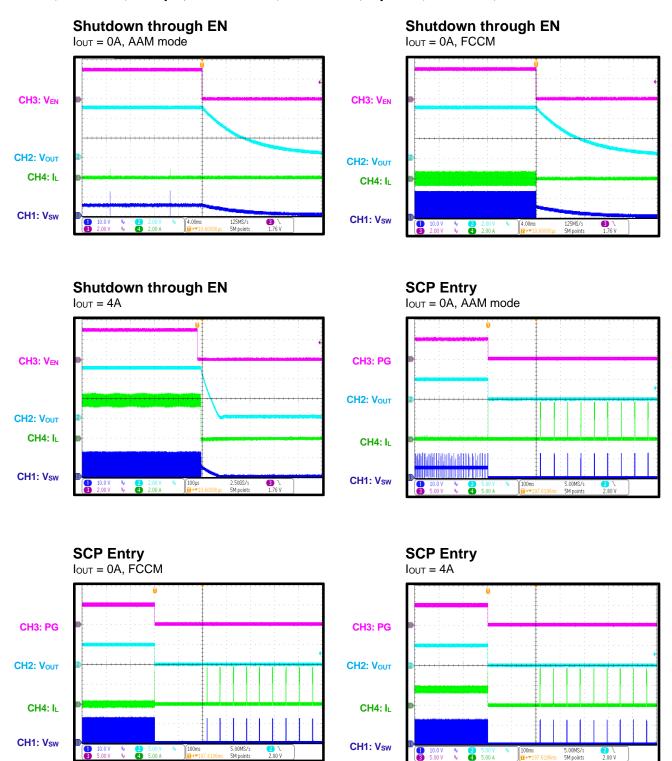


 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $L = 1\mu H$ ,  $f_{SW} = 2.2MHz$ , AAM mode, 1-phase,  $T_A = 25$ °C, unless otherwise noted.





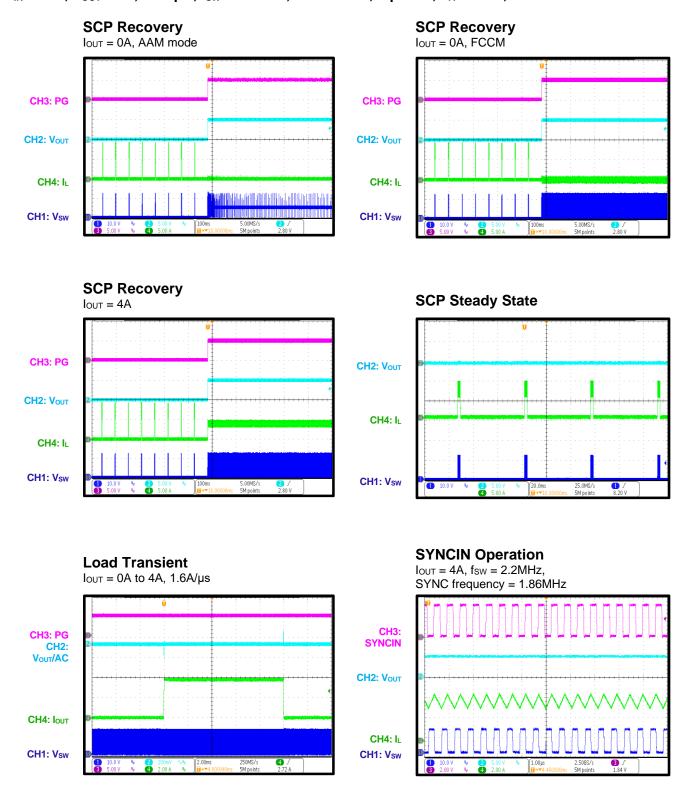
 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $L = 1\mu H$ ,  $f_{SW} = 2.2MHz$ , AAM mode, 1-phase,  $T_A = 25$ °C, unless otherwise noted.



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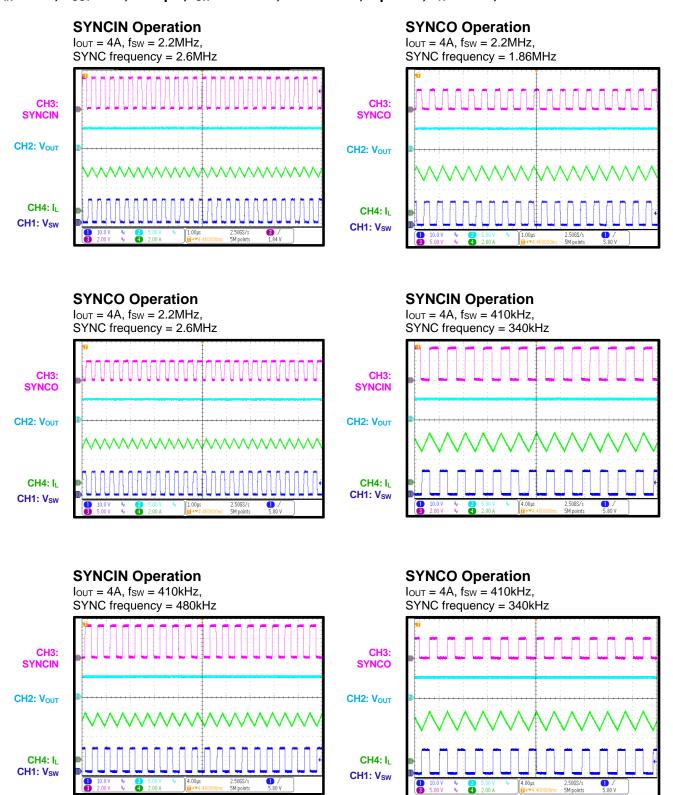


 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ , L = 1 $\mu$ H,  $f_{SW} = 2.2$ MHz, AAM mode, 1-phase,  $T_A = 25$ °C, unless otherwise noted.





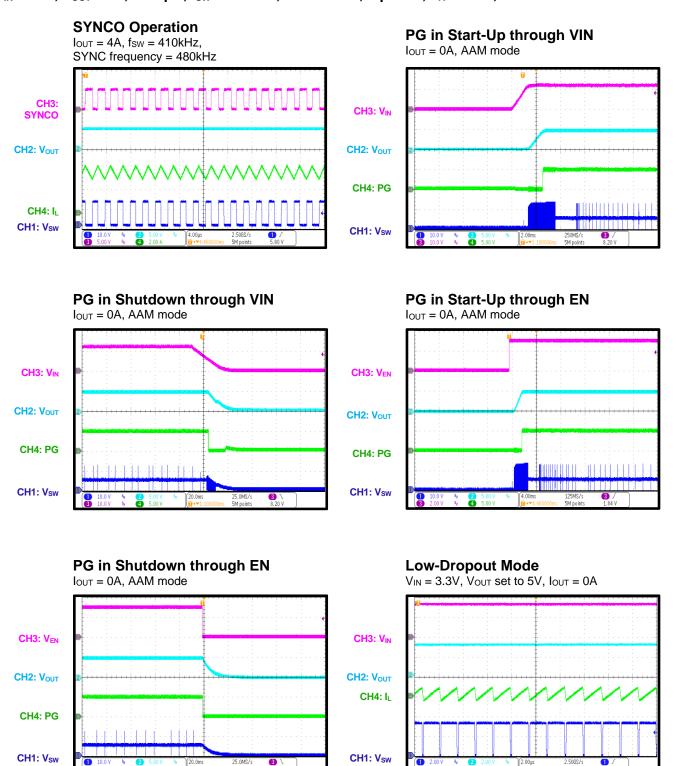
 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ , L = 1 $\mu$ H,  $f_{SW} = 2.2$ MHz, AAM mode, 1-phase,  $T_A = 25$ °C, unless otherwise noted.



31



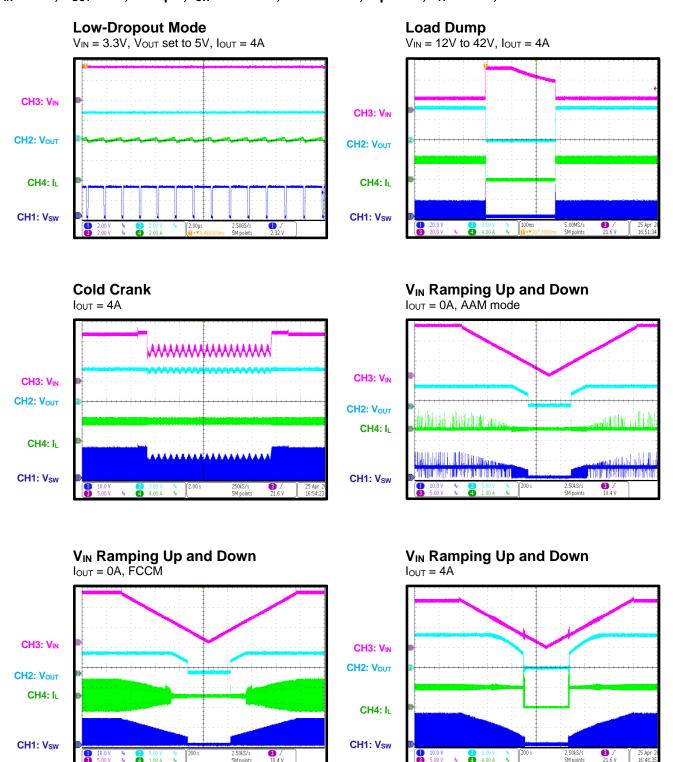
 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ , L = 1 $\mu$ H,  $f_{SW} = 2.2$ MHz, AAM mode, 1-phase,  $T_A = 25$ °C, unless otherwise noted.



32

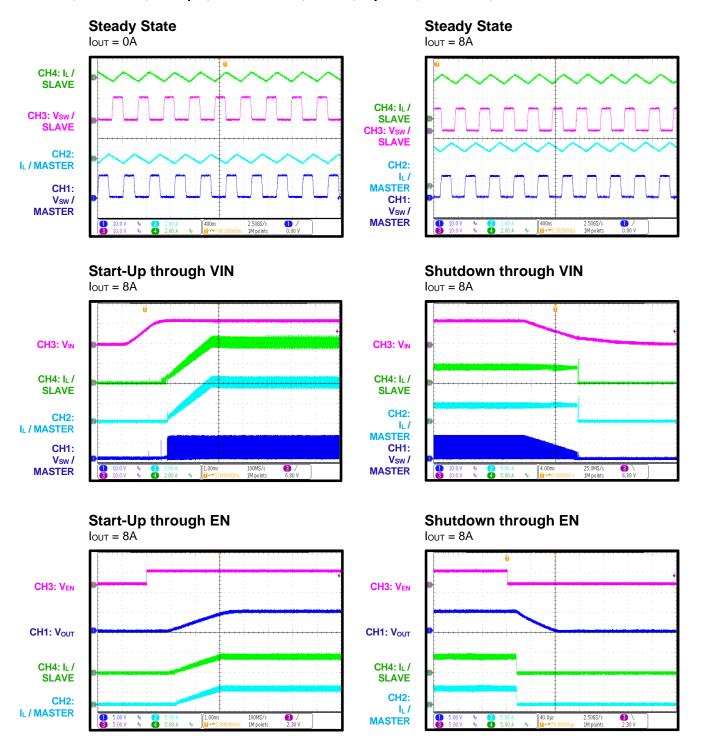


 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ , L = 1 $\mu$ H,  $f_{SW} = 2.2MHz$ , AAM mode, 1-phase,  $T_A = 25$ °C, unless otherwise noted.





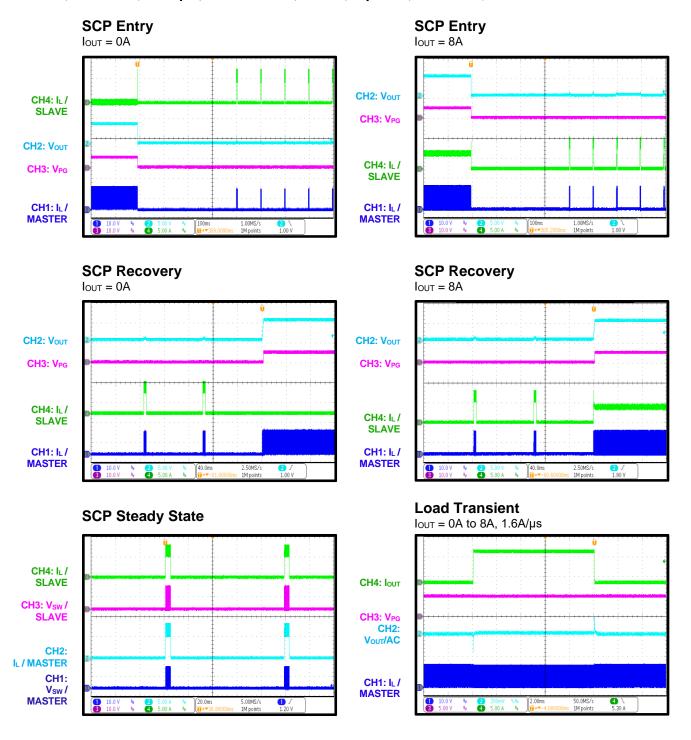
 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H,  $f_{SW}$  = 2.2MHz, FCCM, 2-phase,  $T_A$  = 25°C, unless otherwise noted.



34

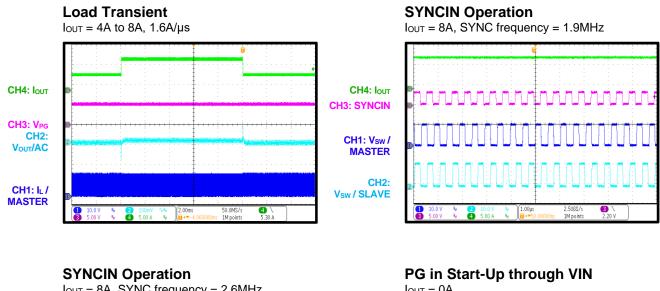


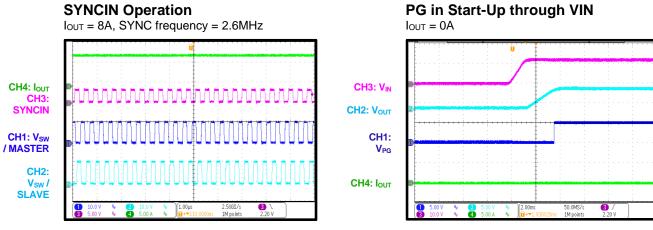
 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ , L = 1 $\mu$ H,  $f_{SW} = 2.2MHz$ , FCCM, 2-phase,  $T_A = 25$ °C, unless otherwise noted.

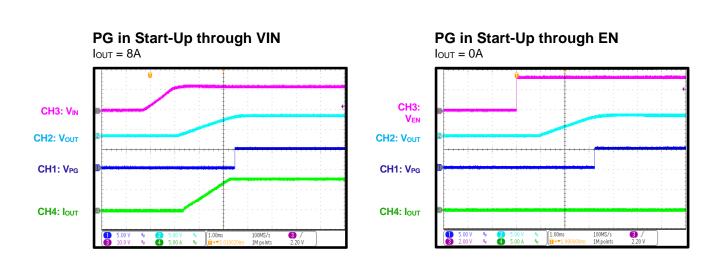




 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H,  $f_{SW}$  = 2.2MHz, FCCM, 2-phase,  $T_A$  = 25°C, unless otherwise noted.



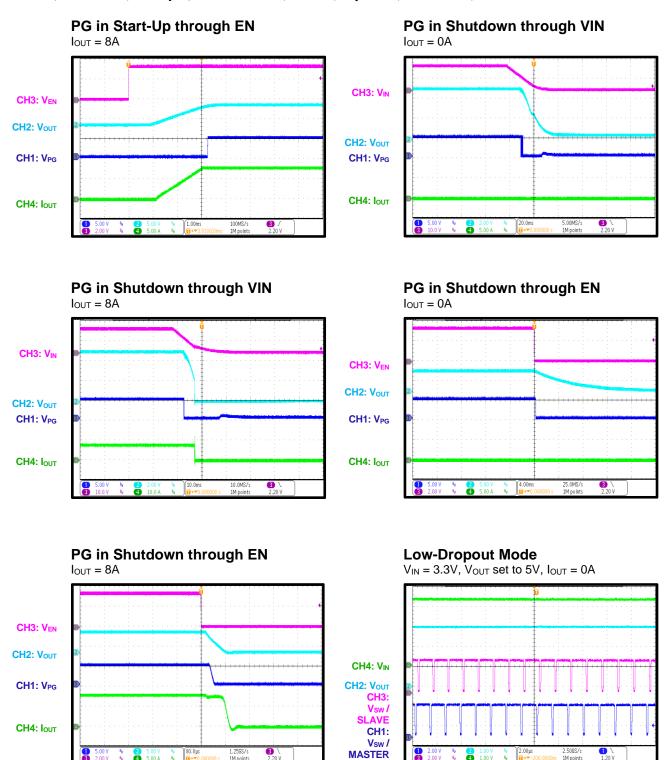






## TYPICAL PERFORMANCE CHARACTERISTICS (continued)

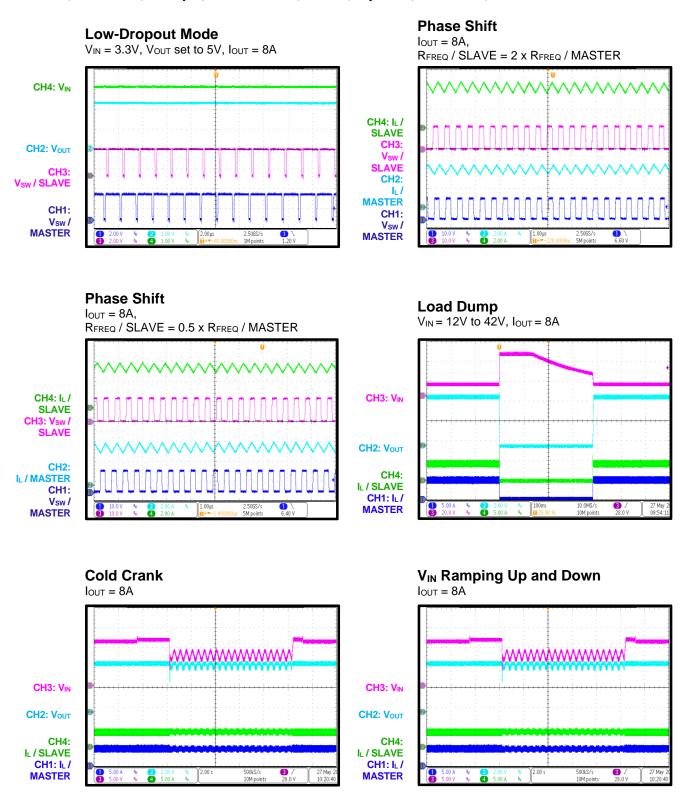
 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V, L = 1 $\mu$ H,  $f_{SW}$  = 2.2MHz, FCCM, 2-phase,  $T_A$  = 25°C, unless otherwise noted.





### TYPICAL PERFORMANCE CHARACTERISTICS (continued)

 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ , L = 1 $\mu$ H,  $f_{SW} = 2.2$ MHz, FCCM, 2-phase,  $T_A = 25$ °C, unless otherwise noted.





## **FUNCTIONAL BLOCK DIAGRAM**

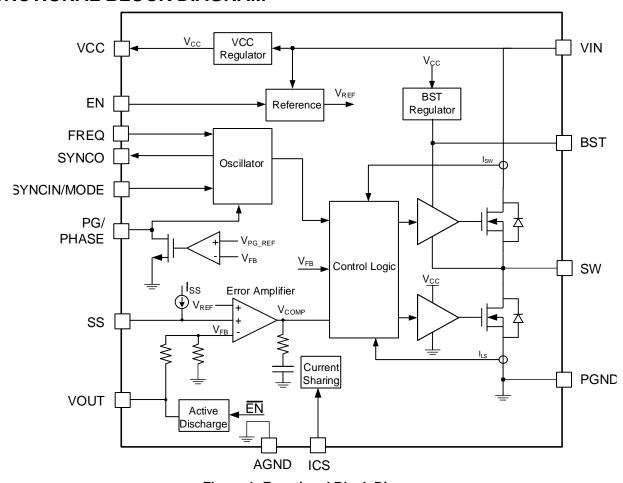


Figure 1: Functional Block Diagram



#### **OPERATION**

The MPQ4340/4340J is a synchronous, step-down switching converter with integrated internal high side and low side power MOSFETs (HSFETs and LS-FETs, respectively). It provides up to 4A of highly efficient output current (I<sub>OUT</sub>) with fixed-frequency, zero-delay pulse-width module (PWM) control.

The device features wide input voltage ( $V_{IN}$ ) range, configurable 350kHz to 2.5MHz switching frequency ( $f_{SW}$ ), external soft start, and precision current limiting. Its very low operational quiescent current ( $I_Q$ ) makes the MPQ4340/4340J well-suited for battery-powered applications.

## Zero-Delay Pulse-Width Modulation (PWM) Control (ZDP)

Automotive applications typically require fixed-frequency operation to reduce EMI, but traditional fixed-frequency control topologies have major limitations. Voltage mode is difficult to compensate in automotive environments, while peak current mode control struggles to keep up with stringent, modern system-on-chip (SoC) transient requirements without excessive output capacitance. With these requirements in mind, the MPQ4340/4340J introduces fixed-frequency zero-delay PWM control (ZDP).

ZDP combines current information with hysteretic-style output voltage (V<sub>OUT</sub>) control in a clocked system. This provides near-optimal transient response, while maintaining a high phase margin across a wide variety of operating conditions and external component values. It also maintains superior EMI performance. The improved transient response reduces output capacitor requirements, lowering system cost. Trailing-edge modulation is used to facilitate a narrow minimum on-time (t<sub>ON\_MIN</sub>) for high conversion ratio applications.

At the beginning of the PWM cycle, the HS-FET turns off and the LS-FET turns on immediately, then remains on until the control signal reaches the COMP voltage ( $V_{\text{COMP}}$ ). The HS-FET remains off for at least 120ns at the beginning of the cycle.

#### **Light-Load Operation**

At moderate to high output currents, the MPQ4340/4340J operates with a fixed

frequency. Under light-load conditions, the device can work in two different operation modes by setting the state of the SYNCIN/MODE pin.

When the SYNCIN/MODE pin is pulled above 1.8V or an external clock is used, the MPQ4340/4340J works in forced continuous conduction mode (FCCM). In this mode, it works with a fixed frequency from no-load to full-load conditions. The part has a reverse current limit (about -4A) to prevent the negative current from dropping too low and potentially damaging the components. Once the negative inductor current reaches the reverse current (I<sub>LIMIT REVERSE</sub>), the HS-FET immediately turns on and the LS-FET turns off. The advantage of FCCM is its constant frequency and lower output voltage ripple at light loads.

When the SYNCIN/MODE pin is pulled below 0.4V, the MPQ4340/4340J works in advanced asynchronous modulation (AAM) mode. The device cannot enter AAM mode until soft start (SS) finishes. AAM mode optimizes efficiency under light-load and no-load conditions.

In AAM mode, the LS-FET emulates a diode and the HS-FET has a fixed one-shot on time to charge the inductor and keep V<sub>OUT</sub> within regulation. As the load decreases, the interval between one-shots increases. When this interval exceeds 8µs, the part enters sleep mode which turns off some internal circuits and extends the on time to achieve an ultra-low IQ. When the load increases and the interval becomes shorter than 6µs, the part exits sleep mode and re-enters AAM mode. During this mode, the part employs a zero-current detection (ZCD) circuit to turn off the LS-FET and prevent negative I<sub>L</sub> flow at light loads. If the MODE pin goes high, the part exits AAM mode. If an over-voltage (OV) or overtemperature (OT) fault occurs in sleep mode, the internal circuits are not disabled.

#### Frequency Spread Spectrum (FSS)

The MPQ4340/4340J uses a 12kHz modulation frequency with fixed 128 steps triangular profile to spread the internal switching frequency ( $f_{SW}$ ) across a 20% ( $\pm 10\%$ ) window. The absolute frequency step size varies proportionally with  $f_{SW}$  to maintain the  $\pm 10\%$  frequency spread (see Figure 2 on page 41).

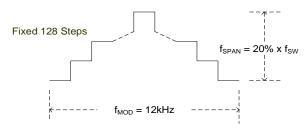


Figure 2: Frequency Spread Spectrum

Sidebands are created by modulating  $f_{SW}$  with the triangle modulation waveform. The emission power of the fundamental  $f_{SW}$  and its harmonics is distributed into smaller pieces, which significantly reduces the peak EMI noise.

#### Low-Dropout (LDO) Mode

When  $V_{\text{IN}}$  drops to about 7V, the MPQ4340/4340J folds back the frequency. When  $V_{\text{IN}}$  is almost equal to  $V_{\text{OUT}}$ , the IC enters low-dropout (LDO) mode.

The effective duty cycle during the regulator's dropout period is mainly influenced by the voltage drops across the MOSFET, the inductor resistance, the low-side diode, and the PCB resistance.

### Start-Up and Shutdown

If both  $V_{\text{IN}}$  and the EN voltage ( $V_{\text{EN}}$ ) exceed their respective thresholds, the device starts up. The reference block starts first, generating a stable reference voltage and currents, and then the internal regulator is enabled. The regulator provides a stable supply for the remaining circuitries.

While the internal supply rail is up, an internal timer holds the MOSFET off for about 50µs to blank any start-up glitches. When the SS block is enabled, it first holds its SS output low to ensure the remaining circuits are ready, then slowly ramps up.

Three events can shut down the chip: EN going low,  $V_{\text{IN}}$  going low, and thermal shutdown. During the shutdown procedure, the signaling path is blocked first to avoid any fault triggering. Then  $V_{\text{COMP}}$  and the internal supply rail are pulled down. The floating driver is not subject to this shutdown command, but its charging path is disabled.

#### SYNCIN and SYNCO

 $f_{\text{SW}}$  can be synchronized to the rising edge of a clock signal applied to the SYNCIN/MODE pin. The recommended SYNCIN frequency range is between 90% and 115% of  $f_{\text{SW}}$ .

The SYNCO pin can output a clock signal in phase with the internal oscillator when there is no SYNCIN signal, or it can output a clock signal in phase with SYNCIN if an external clock signal is applied at SYNCIN (see Figure 3). This makes enabling a dual-phase, interleaved configuration easy (see Figure 4).

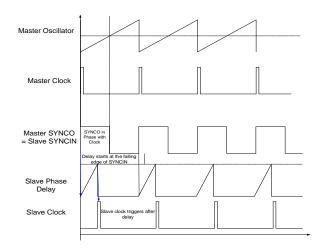


Figure 3: SYNCIN and SYNCO Scheme

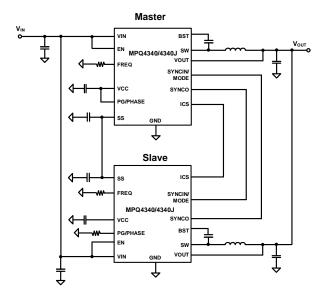


Figure 4: 2-Phase Configuration



For multi-phase applications, the VOUT and ICS pins of the chips in parallel must be connected together, respectively (see Figure 5). Connect the SYNCO pin of the master device to the SYNCIN/MODE pins of the slave devices being interleaved. The SYNCO pins of the slaves can be tied to the SYNCIN/MODE pin of the master device to select the mode of the slave devices. Place a resistor to AGND near the PG/PHASE pin of each slave to set the phase delay, enabling simple multi-phase operation. Short the PG/PHASE pin of the slave devices to set no delay on the SYNCIN signal.

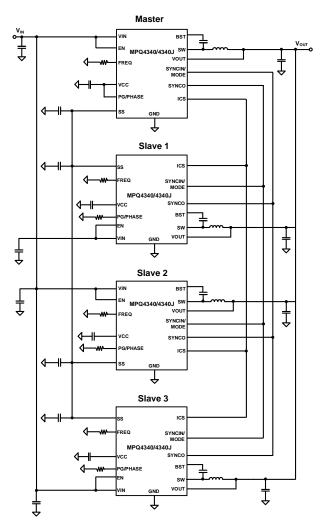


Figure 5: 4-Phase Configuration

#### Thermal Shutdown

Thermal shutdown is implemented to protect the chip from thermal runaway. When the silicon die temperature exceeds its upper threshold (170°C), the power MOSFETs shut down. Once the temperature drops below its lower threshold (150°C), the thermal shutdown condition is removed and the chip starts up again.



### **APPLICATION INFORMATION**

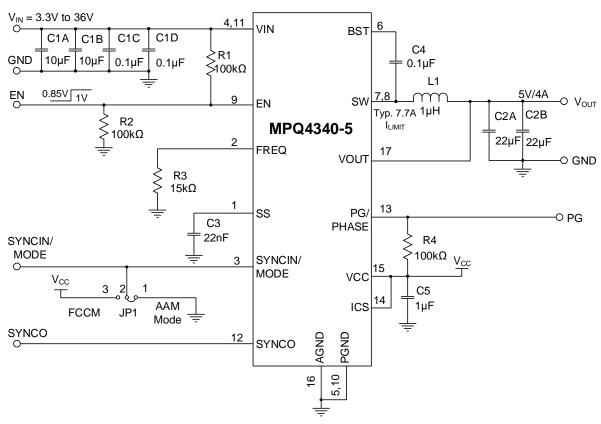


Figure 6: Typical Application Circuit for the MPQ4340GLE-5 (V<sub>OUT</sub> = 5V, f<sub>SW</sub> = 2.2MHz)

**Table 1: Design Guide Index** 

Pin#	Pin Name	Component	Design Guide Index
1	SS	C3	Selecting the Soft-Start Capacitor (SS, Pin 1)
2	FREQ	R3	Setting the Switching Frequency (f <sub>SW</sub> ) (FREQ, Pin 2)
3	SYNCIN/MODE	-	SYNC Input and MODE Selection (SYNCIN/MODE, Pin 3)
4, 11	VIN	C1A, C1B, C1C, C1D	Selecting the Input Capacitors (VIN, Pins 4 and 11)
5, 10	PGND	-	GND Connection (GND, Pins 5, 10, and 16)
6	BST	C4	Floating Driver and Bootstrap Charging (BST, Pin 6)
7, 8	SW	L1, C2A, C2B	Selecting the Inductor (SW, Pins 7 and 8)
7, 0			Selecting the Output Capacitors (SW, Pins 7 and 8)
9	EN	R1, R2	Enable and V <sub>IN</sub> Under-Voltage Lockout (UVLO) (EN, Pin 9)
12	SYNCO	-	SYNCO (Pin 12)
13	PG/PHASE	R4	Power Good (PG) Indicator and Phase Shift (PG/PHASE, Pin 13)
14	ICS	-	Current Sharing (ICS, Pin 14)
15	VCC	C5	Input Bias Supply (VCC, Pin 15)
16	AGND	-	GND Connection (GND, Pins 5, 10, and 16)
17	VOUT	-	VOUT (Pin 17)



#### Selecting the Soft-Start Capacitor (SS, Pin 1)

Soft start (SS) is implemented to prevent the converter's V<sub>OUT</sub> from overshooting during startup.

When SS begins, an internal current source begins charging the external SS capacitor (C<sub>SS</sub>). When the SS voltage (V<sub>SS</sub>) is below the internal reference voltage (V<sub>REF</sub>), V<sub>SS</sub> overrides V<sub>REF</sub>, so the error amplifier (EA) uses V<sub>SS</sub> as the reference. When V<sub>SS</sub> exceeds V<sub>REF</sub>, V<sub>REF</sub> regains control.

C<sub>SS</sub> can be calculated with Equation (1):

$$C_{SS}(nF) = \frac{t_{SS}(ms) \times I_{SS}(\mu A)}{V_{RFF}(V)} = 16.6 \times t_{SS}(ms)$$
 (1)

The SS pin can be used for tracking and sequencing.

## Setting the Switching Frequency (f<sub>SW</sub>) (FREQ,

fsw can be configured by an external resistor connected from the FREQ pin to ground, placed as close to the device as possible.

The resistance that sets f<sub>SW</sub> (R3) can be selected using the f<sub>SW</sub> vs R<sub>FREQ</sub> curves. Figure 7 shows the f<sub>SW</sub> vs. R<sub>FRFQ</sub> curve when f<sub>SW</sub> is between 1000kHz and 2500kHz.

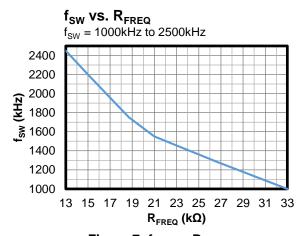


Figure 7: fsw vs. RFREQ

Figure 8 shows the f<sub>SW</sub> vs. R<sub>FREQ</sub> curve when f<sub>SW</sub> is between 350kHz and 1000kHz.

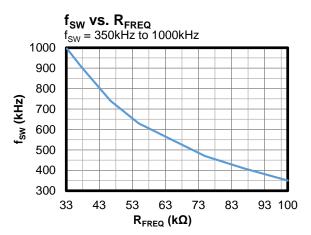


Figure 8: fsw vs. RFREQ

Table 2 shows some common f<sub>SW</sub> and R<sub>FREQ</sub> values when selecting fsw.

Table 2: fsw vs. RFREQ

R <sub>FREQ</sub> (kΩ)	fsw (kHz)
100	350
86.6	410
75	470
64.9	550
54.9	630
46.4	740
37.4	910
33	1050
26.7	1280
21	1550
18.7	1750
15	2200
13	2450

#### SYNC MODE Input and Selection (SYNCIN/MODE, Pin 3)

When the SYNCIN/MODE pin is used as the SYNC input pin (SYNCIN), f<sub>SW</sub> can be synchronized to the rising edge of a clock signal applied to SYNCIN/MODE. The recommended SYNCIN frequency range is 90% to 115% of f<sub>SW</sub>.

When SYNCIN/MODE is used for mode selection (MODE), pulling this pin high allows the device to operate in FCCM, while pulling it low allows the device to operate in AAM mode (see Table 3 on page 45).



**Table 3: Mode Selection** 

SYNCIN/MODE Input	Operation Mode		
<0.4V	AAM mode		
>1.8V	FCCM		
External clock in	FCCM		

## Selecting the Input Capacitor (VIN, Pins 4 and 11)

The step-down converter has a discontinuous input current, and requires a capacitor to supply AC current to the converter while maintaining the DC  $V_{\text{IN}}$ . For the best performance, use low-ESR capacitors. Ceramic capacitors with X5R or X7R dielectrics are highly recommended because of their low ESR and small temperature coefficients.

For most applications, it is recommended to use a  $4.7\mu F$  to  $10\mu F$  capacitor. It is strongly recommended to use another, lower-value capacitor (e.g.  $0.1\mu F$ ) with a small package size (0603) to absorb high-frequency switching noise. Place the smaller capacitor as close to VIN and GND as possible.

Since the input capacitor ( $C_{IN}$ ) absorbs the input switching current, it requires an adequate ripple current rating. The RMS current for  $C_{IN}$  ( $I_{CIN}$ ) can be estimated with Equation (2):

$$I_{CIN} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times (1 - \frac{V_{OUT}}{V_{IN}})}$$
 (2)

The worst-case condition occurs at  $V_{IN} = 2 x V_{OUT}$ , which can be calculated with Equation (3):

$$I_{CIN} = \frac{I_{LOAD}}{2}$$
 (3)

For simplification, choose an input capacitor with an RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum, or ceramic. When using electrolytic or tantalum capacitors, add a small, high-quality ceramic capacitor (e.g. 0.1µF) as close to the IC as possible. When using ceramic capacitors, ensure that they have enough capacitance to provide a sufficient charge to prevent excessive voltage ripple at the input.

The input voltage ripple ( $\Delta V_{IN}$ ) caused by the capacitance can be estimated with Equation (4):

$$\Delta V_{IN} = \frac{I_{LOAD}}{f_{SW} \times C_{IN}} \times \frac{V_{OUT}}{V_{IN}} \times (1 - \frac{V_{OUT}}{V_{IN}})$$
 (4)

When  $V_{IN}$  is above 25V, the device allows the  $V_{IN}$  OVP circuit to turn on. See the  $V_{IN}$  Over-Voltage Protection (OVP) section on page 48 for more details.

### GND Connection (Pins 5, 10, and 16)

See the PCB Layout Guidelines section on page 49 for more details.

## Floating Driver and Bootstrap Charging (BST, Pin 6)

The bootstrap (BST) capacitor (C4) is recommended to be between 0.1µF and 0.22µF.

It is not recommended to place a resistor (RBST) in series with the BST capacitor (CBST) unless there is a strict EMI requirement. RBST helps enhance EMI performance and reduce voltage stress at high input voltages, but it also increases power consumption and reduces efficiency. When RBST is necessary, it should be below  $10\Omega$ .

C<sub>BST</sub> is charged and regulated to about 5V by the dedicated internal BST regulator. When the voltage between the BST and SW nodes is below its regulation, an N-channel MOSFET pass transistor connected from VCC to BST turns on to charge C<sub>BST</sub>. The external circuit should provide sufficient voltage headroom to facilitate charging.

When the HS-FET is on, the BST voltage ( $V_{\text{BST}}$ ) exceeds  $V_{\text{CC}}$ , so  $C_{\text{BST}}$  cannot be charged.

At higher duty cycles, the time available for bootstrap charging is shorter, so  $C_{\text{BST}}$  may not be sufficiently charged. If the external circuit has both insufficient voltage and time to charge  $C_{\text{BST}}$ , use additional external circuitry to ensure  $V_{\text{BST}}$  remains within the normal operation range.

#### Selecting the Inductor (SW, Pins 7 and 8)

A 1µH to 10µH inductor with a DC current rating at least 25% greater than the maximum load current is recommended for most applications. For higher efficiency, choose an inductor with a lower DC resistance. A larger-value inductor results in less ripple current and a lower output ripple voltage, but also has a larger physical size,



higher series resistance, and lower saturation current. A good rule for determining the inductor value is to allow the inductor ripple current to be approximately 30% of the maximum load current. The inductance value can be calculated with Equation (5):

$$L = \frac{V_{OUT}}{f_{SW} \times \Delta I_{L}} \times (1 - \frac{V_{OUT}}{V_{IN}})$$
 (5)

Where  $\Delta I_L$  is the peak-to-peak inductor ripple current.

Choose the inductor ripple current to be approximately 30% of the maximum load current. The maximum peak inductor current ( $I_{LP}$ ) can be calculated with Equation (6):

$$I_{LP} = I_{LOAD} + \frac{V_{OUT}}{2f_{SW} \times L} \times (1 - \frac{V_{OUT}}{V_{IN}})$$
 (6)

## Selecting the Output Capacitor (SW, Pins 7 and 8)

The output capacitor ( $C_{OUT}$ ) maintains the DC  $V_{OUT}$ . Use ceramic, tantalum, or low-ESR electrolytic capacitors. For the best results, use low-ESR capacitors to keep the output voltage ripple ( $\Delta V_{OUT}$ ) low.  $\Delta V_{OUT}$  can be estimated with Equation (7):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times L} \times (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}) \times (R_{\text{ESR}} + \frac{1}{8 \times f_{\text{SW}} \times C_{\text{OUT}}}) (7)$$

Where L is the inductance, and  $R_{\text{ESR}}$  is the equivalent series resistance (ESR) value of  $C_{\text{OUT}}$ .

For ceramic capacitors, the capacitance dominates the impedance at  $f_{SW}$  and causes the majority of  $\Delta V_{OUT}$ . For simplification,  $\Delta V_{OUT}$  can be estimated with Equation (8):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{8 \times f_{\text{SW}}^2 \times L \times C_{\text{OUT}}} \times (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}})$$
 (8)

For tantalum or electrolytic capacitors, the ESR dominates the impedance at  $f_{SW}$ . For simplification,  $\Delta V_{OUT}$  can be estimated with Equation (9):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times L} \times (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}) \times R_{\text{ESR}} \tag{9}$$

The  $C_{\text{OUT}}$  characteristics also affect the stability of the regulation system. The part can be

optimized for a wide range of capacitances and ESR values.

# Enable and V<sub>IN</sub> Under-Voltage Lockout (UVLO) (EN, Pin 9)

EN is a digital control pin that turns the regulator on and off.

### Enabled by External Logic High/Low Signal

When the EN voltage ( $V_{EN}$ ) reaches about 0.7V, the VCC supply turns on. When  $V_{IN}$  exceeds 2.7V, it provides an accurate reference voltage for the EN threshold. Forcing EN above its 1V rising threshold turns on the device. Driving EN below 0.85V turns off the device.

## Configurable V<sub>IN</sub> Under-Voltage Lockout (UVLO)

When  $V_{\text{IN}}$  is sufficiently high, the chip can be enabled and disabled via the EN pin. An internal pull-down resistor in this circuit can generate a configurable  $V_{\text{IN}}$  under-voltage lockout (UVLO) and hysteresis.

The device requires a higher voltage ( $\geq 3.3V$ ) for  $V_{IN}$  to directly start up. The part has an internal, fixed UVLO threshold. The rising threshold is 3V, while the falling threshold is about 2.8V. For applications that require a higher UVLO point, an external resistor divider placed between VIN and EN can raise the equivalent UVLO threshold (see Figure 9).

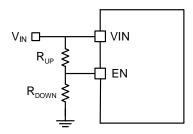


Figure 9: Adjustable UVLO Using EN Divider

The UVLO rising threshold (V<sub>IN\_UVLO\_RISING</sub>) can be calculated with Equation (10):

$$V_{\text{IN\_UVLO\_RISING}} = (1 + \frac{R_{\text{UP}}}{R_{\text{DOWN}}}) \times V_{\text{EN\_RISING}}$$
 (10)

The UVLO falling threshold (V<sub>IN\_UVLO\_FALLING</sub>) can be calculated with Equation (11):

$$V_{\text{IN\_UVLO\_FALLING}} = \left(1 + \frac{R_{\text{UP}}}{R_{\text{DOWN}}}\right) \times V_{\text{EN\_FALLING}} \quad (11)$$



Where  $V_{EN\_RISING}$  is 1V, and  $V_{EN\_FALLING}$  is 0.85V.

#### SYNCO (Pin 12)

During start-up, the MPQ4340/4340J checks the SYNCO pin's status to confirm whether the part is intended to operate in master or slave mode. If the SYNCO is in a high-impendence (Hi-Z) state, the part acts as a master; if not, the part acts as a slave device.

If the part is operating as a master, SYNCO can be left floating. When operating as a master, SYNCO outputs a clock signal in phase with the internal oscillator signal or the external SYNCIN clock.

If SYNCO is connected to AGND, external voltage, or an external clock, the part operates as a slave device. In this mode, SYNCO can be pulled high or low to select the mode.

## Power Good (PG) Indicator and Phase Shift (PG/PHASE, Pin 13)

When operating as a master device, the value of the power good (PG) resistor (R4, also called  $R_{PG}$ ) is recommended to be about  $100k\Omega.$  The device includes an open-drain power good (PG) output that indicates whether the regulator's output is within its nominal  $V_{\text{OUT}}$  range. If using PG, connect it to a logic high power source (e.g. 3.3V) via a pull-up resistor. If the  $V_{\text{OUT}}$  is within 94% to 106% of its nominal voltage, PG goes high. If  $V_{\text{OUT}}$  exceeds 107% or is below 93% of its nominal voltage, PG goes low. Float PG if it is not used.

When operating as a slave device, the PG/PHASE pin can be used to set the phase shift by connecting  $R_{PG}$  to AGND. The phase shift phase can be calculated using Equation (12):

Phase Shift = 
$$\frac{RPG}{R_{FREQ}} \times 180^{\circ}$$
 (12)

#### **Current Sharing (ICS, Pin 14)**

The ICS pin's voltage exceeds 2.4V, current sharing is disabled. Connect this pin to VCC to disable current sharing for single-phase applications.

For multi-phase applications, connect the ICS pins of the devices in parallel.

#### **Setting the VCC Capacitor (VCC, Pin 15)**

Most of the internal circuitry is powered by the internal, 5V VCC regulator. This regulator uses  $V_{\text{IN}}$  as its input and operates across the full  $V_{\text{IN}}$  range. When  $V_{\text{IN}}$  exceeds 5V,  $V_{\text{CC}}$  is in full regulation. When  $V_{\text{IN}}$  is below 5V, the output  $V_{\text{CC}}$  degrades.

The VCC capacitor ( $C_{VCC}$ ) should have a capacitance at least 10 times greater than the boost capacitor, and at least 1 $\mu$ F nominally. A  $C_{VCC}$  above 68 $\mu$ F nominal is not recommended.

#### VOUT (Pin 17)

Because the feedback resistor divider is integrated internally, connect the VOUT pin directly to the output (see Figure 10).

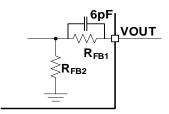


Figure 10: Feedback Divider Network for Fixed-Output Version

The following fixed outputs can be selected: 1V, 1.1V, 1.8V, 2.5V, 3V, 3.3V, 3.8V, or 5V.

Table 4 shows the relationship between the internal  $R_{\text{FB}}$  and  $V_{\text{OUT}}$ .

R<sub>FB2</sub> (MΩ) R<sub>FB1</sub> (MΩ) V<sub>OUT</sub> (V) 1 1.33 2 1.1 1.67 2 2 1.8 4 2.5 6.33 2 3 8 2 9 2 3.3 10.67 2 3.8

14.67

2

Table 4: R<sub>FB</sub> vs. V<sub>OUT</sub>

#### **Peak and Valley Current Limits**

5

Both the HS-FET and LS-FET have cycle-by-cycle current-limit protection. If the inductor current ( $I_L$ ) reaches the high-side (HS) peak current limit (typically 7.7A) or the rising edge of the internal clock is reached while the current is rising and the HS-FET is on, then the HS-FET is forced off immediately to prevent the current from rising further. When the LS-FET is on, the valley current limit circuit block the PWM from



turning on the HS-FET until  $I_L$  returns to below the low-side (LS) valley current limit (typically 5.9A). This current limit scheme prevents current runaway if an overload or short-circuit event occurs.

#### **Short-Circuit Protection (SCP)**

If the output is shorted to ground,  $V_{\text{OUT}}$  drops below 70% of its nominal output, and the LS-FET current exceeds the 5.9A valley current limit, then the IC turns on the LS-FET until  $I_{\text{L}}$  is fully discharged. The device also begins slowly discharging  $C_{\text{SS}}$ . Once  $C_{\text{SS}}$  is fully discharged, the device restarts with a full SS. This hiccup process repeats until the fault is removed.

## Output Over-Voltage Protection (OVP) and Discharge

There is an internal  $V_{\text{OUT}}$  OVP circuit. If the device is operating in discontinuous conduction mode (DCM) and  $V_{\text{OUT}}$  exceeds 106% of the target voltage, an output discharge path from VOUT to PGND is activated to discharge  $V_{\text{OUT}}$ . The output discharge path remains activated until  $V_{\text{OUT}}$  returns to its regulated value, at which point the device begins switching.

If the device is operating in FCCM and  $V_{\text{OUT}}$  exceeds 106% of the target voltage, the output discharge path turns on. If the negative current limit is triggered 265 times, the part enters hiccup mode and switching stops. Once  $V_{\text{OUT}}$  drops to or below 105% of the target value, a new SS cycle begins. The  $V_{\text{OUT}}$  discharge path remains on until  $V_{\text{OUT}}$  returns to its regulated value, at which point the device begins switching.

#### **VIN Over-Voltage Protection (OVP)**

The MPQ4340/4340J has a built-in  $V_{\text{IN}}$  overvoltage protection (OVP) circuit.  $V_{\text{IN}}$  OVP becomes active at 25V. When  $V_{\text{IN}}$  exceeds the OVP threshold (typically 38V), the LS-FET turns on until  $I_{\text{L}}$  is fully discharged, and then switching stops. When  $V_{\text{IN}}$  drops to the over-voltage (OV) falling threshold (typically 28V) and the hiccup restart delay time expires, the device completes a SS cycle and resumes normal regulation.



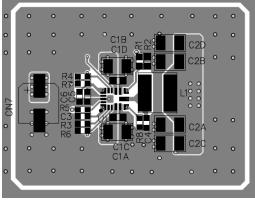
#### PCB Layout Guidelines (12)

Efficient PCB layout is critical for stable operation. A 4-layer layout is strongly recommended to achieve better thermal performance. For best results, refer to Figure 11 and follow the guidelines below:

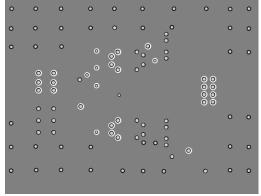
- Place symmetric input capacitors as close to VIN and PGND as possible.
- 2. Connect a large ground plane directly to PGND.
- 3. If the bottom layer is a ground plane, add vias near PGND.
- 4. Ensure that the high-current paths at PGND and VIN have short, direct, and wide traces.
- Place the ceramic input capacitor, especially the small package size (0603) input bypass capacitor, as close to VIN and PGND as possible to minimize high-frequency noise.
- Keep the connection between the input capacitor and VIN as short and wide as possible.
- 7. Place the VCC capacitor as close to VCC and AGND as possible.
- 8. Route SW and BST away from sensitive analog areas, such as FB.
- 9. Use multiple vias to connect the power planes to the internal layers.

#### Note:

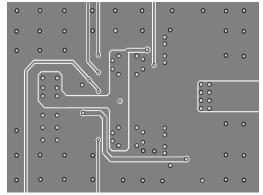
12) The recommended PCB layout is based on Figure 12 on page



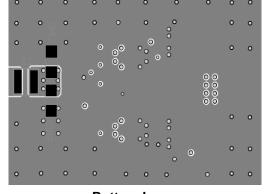
Top Layer



Mid-Layer 1



Mid-Layer 2



Bottom Layer

Figure 10: Recommended PCB Layout



### TYPICAL APPLICATION CIRCUITS

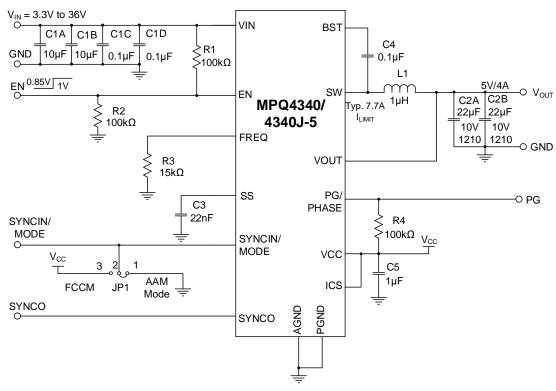


Figure 11: Typical Application Circuit (1-Phase, Vout = 5V, fsw = 2.2MHz)

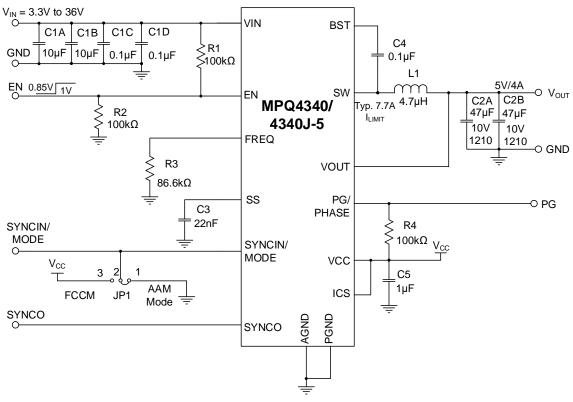


Figure 12: Typical Application Circuit (1-Phase, Vout = 5V, fsw = 410kHz)



## **TYPICAL APPLICATION CIRCUITS (continued)**

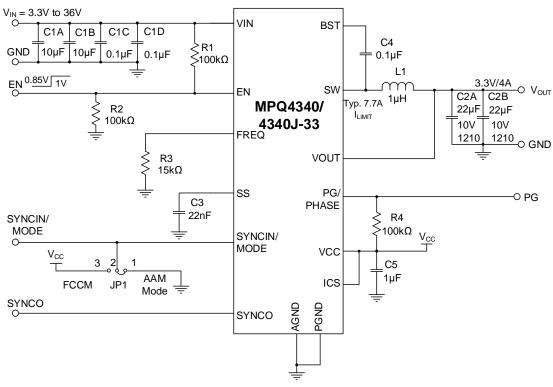


Figure 13: Typical Application Circuit (1-Phase, Vout = 3.3V, fsw = 2.2MHz)

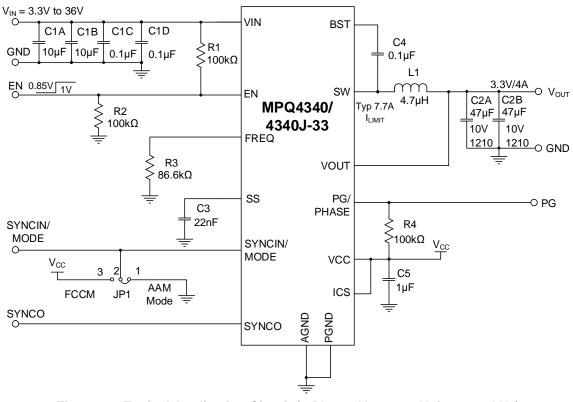


Figure 14: Typical Application Circuit (1-Phase, V<sub>OUT</sub> = 3.3V, f<sub>SW</sub> = 410kHz)



## TYPICAL APPLICATION CIRCUITS (continued)

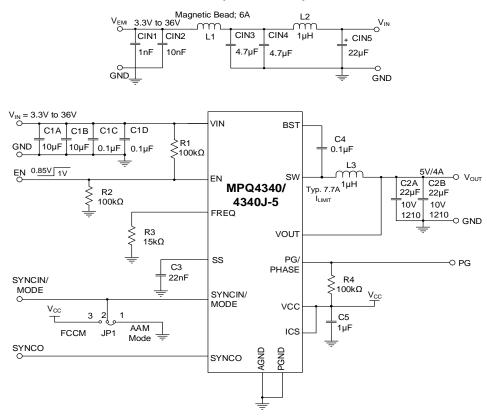


Figure 15: Typical Application Circuit (1-Phase, Vout = 5V, fsw = 2.2MHz with EMI Filter)

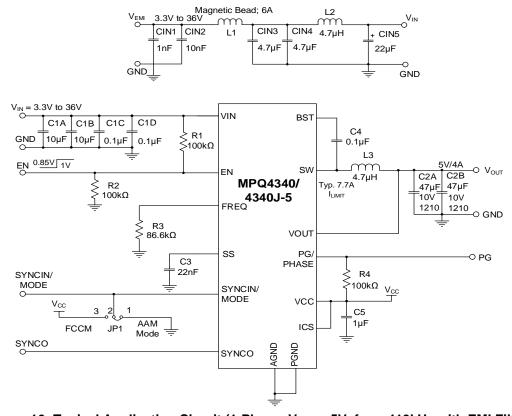


Figure 16: Typical Application Circuit (1-Phase, Vout = 5V, fsw = 410kHz with EMI Filter)

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## TYPICAL APPLICATION CIRCUITS (continued)

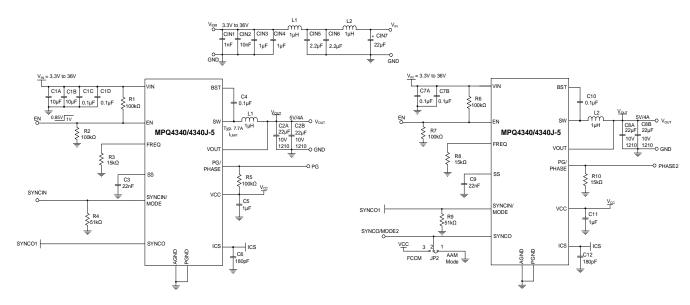


Figure 17: Typical Application Circuit (2-Phase, Vout = 5V, fsw = 2.2MHz with EMI filter)

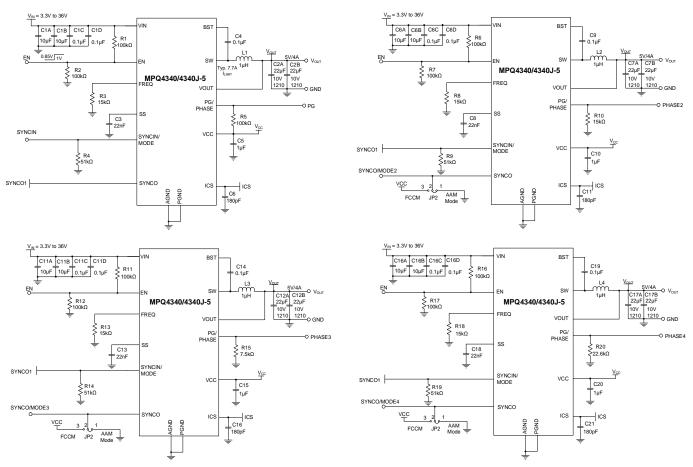
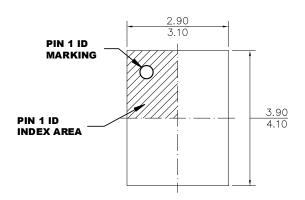


Figure 18: Typical Application Circuit (4-Phase, Vout = 5V, fsw = 2.2MHz)

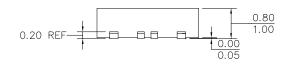


### **PACKAGE INFORMATION**

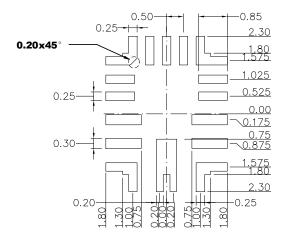
## QFN-17 (3mmx4mm)



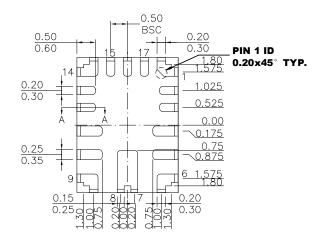
**TOP VIEW** 



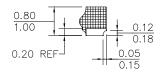
**SIDE VIEW** 



**RECOMMENDED LAND PATTERN** 



**BOTTOM VIEW** 



**SECTION A-A** 

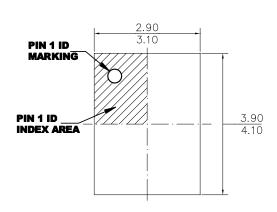
#### NOTE:

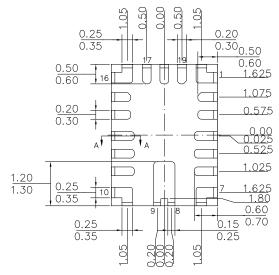
- 1) THE LEAD SIDE IS WETTABLE.
- 2) ALL DIMENSIONS ARE IN MILLIMETERS.
- 3) LEAD COPLANARITY SHALL BE 0.08 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220. 5) DRAWING IS NOT TO SCALE.



## PACKAGE INFORMATION (continued)

### QFN-19 (3mmx4mm)

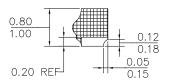




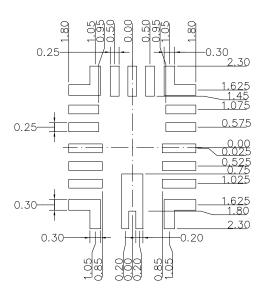
#### **TOP VIEW**







#### SIDE VIEW



**SECTION A-A** 

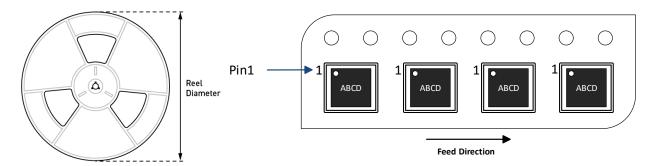
#### **NOTE:**

- 1) THE LEAD SIDE IS WETTABLE.
- 2) ALL DIMENSIONS ARE IN MILLIMETERS.
- 3) LEAD COPLANARITY SHALL BE 0.08 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220.
- 5) DRAWING IS NOT TO SCALE.

**RECOMMENDED LAND PATTERN** 



## **CARRIER INFORMATION**



Part Number	Package Description	Quantity/ Reel	Quantity/ Tube (13)	Quantity/ Tray <sup>(13)</sup>	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MPQ4340GLE-33- AEC1-Z	QFN-17 (3mmx4mm)	5000	N/A	N/A	13in	12mm	8mm
MPQ4340GLE-5- AEC1-Z	QFN-17 (3mmx4mm)	5000	N/A	N/A	13in	12mm	8mm
MPQ4340JGLE- 33-AEC1-Z	QFN-19 (3mmx4mm)	5000	N/A	N/A	13in	12mm	8mm
MPQ4340JGLE-5- AEC1-Z	QFN-19 (3mmx4mm)	5000	N/A	N/A	13in	12mm	8mm

#### Note:

<sup>13)</sup> N/A indicates "not available" in tubes or trays. For 500-piece tape & reel prototype quantities, contact the factory. (The order code for the 500-piece partial reel is "-P"; the tape & reel dimensions remain the same as the full reel.)



### **REVISION HISTORY**

Revision #	Revision Date	Description	Pages Updated
1.0	2/16/2023	Initial Release	-

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